DWLBC REPORT

Groundwater recharge and flow investigations in the Western Mount Lofty Ranges, South Australia

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Department of Water, Land and Biodiversity Conservation

Groundwater recharge and flow investigations in the Western Mount Lofty Ranges, South Australia

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Knowledge and Information Division Department of Water, Land and Biodiversity Conservation

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FOREWORD

South Australia's unique and precious natural resources are fundamental to the economic and social wellbeing of the State. It is critical that these resources are managed in a sustainable manner to safeguard them both for current users and for future generations.

The Department of Water, Land and Biodiversity Conservation (DWLBC) strives to ensure that our natural resources are managed so that they are available for all users, including the environment.

In order for us to best manage these natural resources it is imperative that we have a sound knowledge of their condition and how they are likely to respond to management changes. DWLBC scientific and technical staff continues to improve this knowledge through undertaking investigations, technical reviews and resource modelling.

Rob Freeman CHIEF EXECUTIVE DEPARTMENT OF WATER, LAND AND BIODIVERSITY CONSERVATION

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EXECUTIVE SUMMARY

Technical investigations have been conducted to quantify the various components of the water balance of the Western Mount Lofty Ranges (WMLR), which are essential to the development of the Water Allocation Plan for this area. The most important components to be quantified in the groundwater balance are vertical recharge rates, and horizontal flow velocities. Determining these components in fractured rock aquifers is particularly difficult because the groundwater is stored in, and moves through, fractures and joints in what is essentially impervious rock.

This investigation provides an analysis and quantification of the groundwater recharge and flow rates in the fractured rock aquifer system at selected sites at Forreston, Fox Creek and Mylor in the Torrens and Onkaparinga River Catchments. These will provide sound knowledge with which to estimate recharge rates at a catchment scale and assist in the development of conceptual models of the fractured rock aquifer systems in the WMLR.

Aquifer tests conducted at the Forreston investigation site indicate a freely flowing fractured rock aquifer to a depth of at least 76 m. A recharge model based on groundwater chlorofluorocarbon concentrations indicates a recharge rate at the Forreston site of 44 mm/y. Alternative recharge estimates based on a chloride mass balance model are greater, at 47 mm/y for water at 74 m depth and 61 mm at 18 m depth. Similar hydrochemical compositions throughout the depths sampled suggest that the changes in chloride concentrations with depth are due to changes in the recharge rate over time. Hence an estimate of 61 mm/y for the most recent (shallowest) recharge is taken to be the best approximation of the contemporary recharge rate at this site.

At the Fox Creek investigation site, aquifer tests show a strong hydraulic connection between all depths. The aquifer here has an upward hydraulic gradient between the deepest and shallowest piezometers, and is artesian during the winter. Results of carbon-14 dating of the groundwater indicate a minimum age of ~3600 years, suggesting that water reaches this aquifer via an intermediate flow system. Groundwater here increases in age at greater depths, implying that a slow downward flow has occurred prior to the horizontal flow of water to this location. There is a horizontal flow of up to 19 m/y at a depth of about 40 m, with small horizontal flows above and below that depth. A chloride mass balance recharge estimate of 25 mm/y site is supported by other hydrochemical data for the Fox Creek site and by results from a geologically similar recharge investigation site at Burra.

At the Mylor investigation site, very low yields from the piezometers indicate poor connectivity of fractures in the aquifer. An analysis of radon-222 activities in the groundwater here shows a very low horizontal flow occurring at all depths. These findings indicate that the conductivity of fractures is uniformly low throughout the depth range investigated, and it is likely that the majority of the small flows are horizontal, through fractures that have very few vertical connections. A recharge estimate for this location has been derived from chloride mass balance recharge estimates for groundwater from 14 wells in a nearby area of similar geology. By scaling the mean of these recharge estimates according to the rainfall difference between the location of those wells and the location of the Mylor investigation site, a recharge estimate of 97 mm/y is derived, which is recommended for resource management purposes as a conservative estimate of recharge at locations with geology and rainfall similar to the Mylor investigation site.

1. INTRODUCTION

The Mount Lofty Ranges (MLR) provide important surface and groundwater resources for domestic, industrial and agricultural purposes locally, as well as Metropolitan Adelaide's reticulated water supply. Development and implementation of the Water Allocation Plan (WAP) for the Western Mount Lofty Ranges (WMLR) and Eastern Mount Lofty Ranges (EMLR) Prescribed Water Resources Areas (PWRA) will ensure that current and future development of these resources is sustainable and that the environment is also recognised as a user of the resource.

Technical investigations are being conducted to determine the various components of the water balance in catchments of the WMLR, which are essential to the development of the WAP. The long-term sustainability of the groundwater resource requires careful estimates of the magnitude of all components of the water budget. Important components that need to be quantified are vertical recharge and discharge rates, and horizontal flow velocities. Determining these components in fractured rock aquifers (FRA) is extremely difficult because the groundwater is stored in, and moves through, fractures and joints in what is essentially impervious rock. Traditional investigation techniques applied to sedimentary systems have limited applicability to FRA systems, but several techniques developed recently have been applied to FRA in the Clare Valley (Cook et al. 1999; Cook & Simmons 2000; Love et al. 2002, 2007). These techniques were successful in estimating the components of the groundwater budget and provided sound knowledge in understanding some of the complexities of FRA to develop a conceptual model of the groundwater flow system.

A similar approach has been used in this investigation within the River Torrens Catchment (RTC) and Onkaparinga River Catchment (ORC) as well as other regions in the MLR (Fig. 1.1). The techniques include downhole geophysics, detailed fracture mapping, aquifer pump tests and vertical profiling of groundwater chemistry, isotopes and radioactive tracers. Downhole geophysics was used to indicate physical properties, lithology and porosity of the rock formations. Fracture location, orientation and groundwater flow can also be determined using downhole geophysics. Structural mapping of surface outcrop provided details of fracture spacing and their dominant orientations. Aquifer pump tests provided information on fracture aperture. Groundwater chemistry, specifically chlorofluorocarbon and carbon-14 analyses, provide information on the groundwater age. From this estimated age it is possible to make inferences about the recharge rate — in general, lesser ages indicate relatively high recharge rates, and greater groundwater ages indicate lower recharge rates.

The following investigation aims to provide technical information to support the successful implementation of the WAP for the WMLR.

Specifically, this investigation aims to:

- Estimate the recharge rate to the FRA system at the Forreston and Fox Creek investigation sites in the RTC and at the Mylor investigation site in the Onkaparinga River Catchment.
- Estimate horizontal flow rates at Forreston, Fox Creek and Mylor investigation sites.
- Provide sound knowledge with which to estimate recharge at a catchment scale.
- Assist in the development of a conceptual model of the FRA system in the RTC and ORC.



2. WMLR CATCHMENTS

The RTC covers an area of ~501 km² (Fig. 2.1). The catchment runs in a westerly direction and ranges in elevation from ~700 m AHD at its most southerly margin, dropping sharply to less than 140 m AHD on the western side of the Eden–Burnside Fault, from where the River Torrens traverses the Adelaide Plains and discharges to the sea at West Beach. The catchment contains two major reservoirs at Kangaroo Creek and Millbrook. The major land uses in the catchment are dairying, irrigated pasture for livestock grazing, fruit trees, and viticulture. The western part of the catchment, on the lower side of the Eden–Burnside Fault, is extensively urbanised.

The ORC covers an area of 555 km² and adjoins the southern boundary of the RTC (Fig. 2.1). The catchment ranges in elevation from ~700 m AHD at Mount Lofty down to 10 m AHD at the township of Old Noarlunga, where the Onkaparinga River discharges into the Onkaparinga Estuary. The course of the river is interrupted by the Mount Bold Reservoir in the southwest of the catchment. The major land uses in the catchment are dairying, irrigated pasture for livestock grazing, and some viticulture.

2.1 CLIMATE

The RTC and ORC have similar climatic conditions, with cool wet winters and typically hot dry summers. Annual average rainfall in the RTC ranges from 500–1000 mm/y, with the higher rainfall in the southern part of the catchment, in areas of higher elevation close to Mount Lofty (Fig. 2.1). Rainfall is significantly less in the topographically lower, western reaches of the RTC where the annual average is less than 600 mm/y. The long-term average annual rainfall in the upper part of the RTC, measured at the townships of Gumeracha, Kersbrook and Birdwood, is 799, 739 and 723 mm/y, respectively. Rainfall is winter dominant, falling between the months of April and October.

The majority of the ORC has an average annual rainfall of 800–900 mm/y, except for a section to the northwest of the catchment, toward Mount Lofty, in which the annual average is up to 1200 mm/y. Rainfall is winter dominant, falling between the months of April and October. The long-term average annual rainfall in the upper part of the ORC, measured at the townships of Lobethal, Bridgewater and Echunga, is 886, 1042 and 807 mm/y, respectively.

2.2 GEOLOGY

The geology of the RTC and ORC varies from the Proterozoic Barossa Complex and Adelaidean sequences to the Cambrian Kanmantoo Group (Fig. 2.2).

The Palaeoproterozoic Barossa Complex dominates the northern corner of the RTC, with minor outcrops in the ORC, and forms the basement to the Adelaidean and Cambrian sequences of the Adelaide Geosyncline. Outcrops occur as inliers, thought to represent anticlinal cores, typically with faulted contacts with the overlying Adelaidean sequences. These originally high-grade metamorphic rocks underwent retrograde metamorphism to greenschist facies during the Cambro-Ordovician Delamerian Orogeny (Preiss 1987).





The remaining geology encompasses a significant proportion of the stratigraphic sequence associated with the Adelaide Geosyncline. Outcropping stratigraphic sequences of the Neoproterozoic Burra Group (Emeroo Subgroup, Mundallio Subgroup, Stonyfell Quartzite, Saddleworth Formation and Belair Subgroup), Umberatana Group and Wilpena Group occur in both catchments, as well as the Cambrian Kanmantoo Group. Deformation associated with the Delamerian Orogeny has resulted in north–south-trending, south-plunging folds and complex faulting.

On a local scale, the Forreston investigation site is situated in the Mundallio Subgroup, specifically the Woolshed Flat Shale, of the Burra Group. A fine-grained, quartz–muscovite– schist dominates the geology at this site. Minor quartz vein material and pyrite mineralisation occurs at various depths. Chloritic alteration is observed below depths of 36 m. Weathering appears to be minimal, only extending to 8 m depth, with thin topsoil developed to 2 m.

The Fox Creek investigation site is situated in the Saddleworth Formation of the Burra Group. Slate dominates the geology, with minor occurrences of interbedded metasiltstone and metasandstone. The slate is blue-grey in colour and exhibits a well-developed slaty cleavage. Quartz vein material occurs at depths exceeding 20 m. Pyrite mineralisation, occurring on fracture surfaces and occasionally as discrete veins, occurs below depths of 15 m. Weathering within the slate is observed to depths of ~18 m. A surficial regolith zone, consisting of clay, silty clay and highly weathered slate fragments, extends to ~8 m depth.

The Mylor investigation site is situated in the Emeroo Subgroup, specifically the Aldgate Sandstone, of the basal Burra Group. Quartzite and metasandstone dominate the geology, with minor occurrences of muscovite and biotite–quartz schist. The metasandstone, occurring between 10–25 m, is medium-grained, moderately to well sorted, subrounded–subangular and well cemented. The quartzite is green-grey in colour, crystalline in appearance and well silicified. Possible crenulation cleavage and chloritic alteration can be observed in the mica–quartz schist. Quartz vein material occurs at depths exceeding 10 m. A surficial regolith zone extends to 10 m depth and consists of clay, sand and highly weathered metasandstone fragments. Detailed lithological logs are included in Appendix B.

2.3 HYDROGEOLOGY

Groundwater in both the RTC and ORC exists primarily in FRA within the sedimentary and metasedimentary rocks of the Neoproterozoic Adelaidean sequence. In the northern part of the RTC, around Kersbrook, and in a small area of the ORC, significant FRA exist in metamorphic rocks of the Palaeoproterozoic Barossa Complex. In the eastern extremes of both catchments, groundwater resides in the sedimentary and metamorphic rocks of the Cambrian Kanmantoo Group. To the west of the Eden–Burnside Fault, the FRA systems of the upper catchment discharge into the sedimentary aquifers of the Adelaide Plains. This investigation addresses only the FRA systems in the upper RTC and ORC.

3. DRILLING PROGRAM

Drilling and installation of nested piezometer sites was undertaken at two sites in the TRC and at one site in the ORC.

3.1 SITE SELECTION

Potential drilling sites were assessed using several criteria including existing groundwater data, rainfall distribution, topography, and structural and geological data. In both catchments, potential sites were identified in areas of high rainfall and low topographic relief in order to minimise depth to groundwater. Available groundwater data were assessed to provide an indication of depth to water and areas of higher well yield.

The geology was assessed to determine the dominant lithology of each catchment and, within these broad rock types, areas exhibiting appropriate structural characteristics were targeted. Key structural features included steeply dipping to near-vertical bedding and a well-developed bedding plane parallel fracture set. These properties are important for the application of the parallel plate model in groundwater recharge investigations (refer to section 4.5). Another important factor in site selection was distance from large-scale faults and shear zones. Increased fracture development is typically associated with faulting, and whilst this may result in local areas of increased recharge, it is not representative of catchment-scale processes. Therefore, sites that were a considerable distance from major fault zones, and which met all other requirements, were selected.

3.1.1 RIVER TORRENS CATCHMENT

The available groundwater data indicate that the majority of wells are used for either domestic or irrigation purposes. Groundwater in the FRA is generally of good quality for the majority of the upper RTC. Wells are typically less than 100 m deep and 60% are less than 40 m deep. Well yields range from 0.1–50 L/s, with ~92% of wells yielding between 0.1–13 L/s. Well salinities range from 100 to ~8000 mg/L, but the majority are less than 2000 mg/L and 52% of wells have salinities of less than 1000 mg/L.

The topography of the RTC is dominated by the steep slopes of Adelaidean rocks rising to the southern boundary of the catchment, with younger Kanmantoo Group surface geology more prevalent at the eastern end of the catchment. The lower salinity wells are typically in FRA in the areas of higher elevation to the east of the Eden–Burnside Fault. The far eastern end of the catchment is dominated by the geology of the Kanmantoo Group, and salinity of wells in this area is higher than typical for the upper part of the catchment.

As the Kanmantoo Group geology typically provides low-yielding, poor quality aquifers that are less in demand as a groundwater resource, it was considered beneficial to preferentially locate investigation sites in areas of Adelaidean sequence geology. Two suitable investigation sites were located in the RTC, one within an area of Saddleworth Formation at Fox Creek, and another in an area of Woolshed Flat Shale at Forreston.

3.1.2 ONKAPARINGA RIVER CATCHMENT

Groundwater data for the ORC indicates that the majority of wells are used for either domestic or irrigation purposes. Groundwater is generally of good quality in FRA in the majority of the upper ORC. Wells are typically less than 160 m deep and 67% are less than 100 m deep. Well yields range from 0.1–63 L/s with ~91% of wells yielding between 0.1–13 L/s. Well salinities range from 57 to ~8800 mg/L, but the majority are less than 2000 mg/L, and 68% of wells have salinities of less than 1000 mg/L.

Geology of the ORC is dominated by Adelaidean shale and quartzite sequences, principally the Emeroo Subgroup, Woolshed Flat Shale, Stonyfell Quartzite and the Saddleworth Formation. Similar to the RTC, there is a prevalence of Kanmantoo Group geology in the far eastern end of the catchment and a corresponding decline in groundwater quality in that area. A suitable investigation site was located in an area of Emeroo Subgroup, ~3 km south of Mylor.

3.2 DRILLING

Underdale Drillers Pty Ltd undertook the drilling program from May to November 2005 in the RTC and ORC. An Ingersoll-Rand rotary hammer drill rig was used to drill two wells at each site in the RTC and one in the ORC. Due to the large diameter and depth of the wells, a second air compressor and drilling additives were required on numerous occasions to facilitate the removal of cuttings from the hole.

At each site, the wells were drilled as close as possible to each other to increase the potential for intersecting the same fracture sets. This is considered important if attempts are to be made to correlate chemistry data from shallow depths with deeper depths.

Each well was completed with Class 9 PVC casing to ensure stability of the upper weathered section. The remainder of the well was left as an open-hole completion to enable sonding, geophysical logging, acoustic televiewer logging, and EM Flowmeter testing to be conducted. These analyses were conducted to inform the design of the nested piezometers, which were installed later (refer to section 4.3).

The completion details for each site are outlined in Table 3.1.

Catchment	Easting	Northing	Permit number	Unit number	Total drilled depth (m)	Diameter (mm)	Casing depth (m)
Forreston	308036.6	6147499.7	106396	6628-22353	43.0	203	6.0
Forreston	308036.1	6147493.6	106397	6628-22348	80.0	203	3.0
Fox Creek	302579.9	6139401.9	106399	6628-22476	39.5	254	12.0
Fox Creek	302581.9	6139406.9	106398	6628-22475	89.0	203	13.5
Mylor	295657.4	6120312.1	106401	6627-11279	80.2	203	10.0

Table 3.1 Well completion details for the three investigation sites in the RTC and ORC

3.3 WELL SONDING AND GEOPHYSICAL LOGGING

Geophysical logs, EM Flowmeter and Hydrolab surveys were conducted in the 203 mm and 254 mm holes. Hydrolab refers to a YSI[®] 600XL Series Sonde which is used to measure variations in electrical conductivity (EC), pH and temperature with depth. DWLBC's Geophysical Technical Services Group completed downhole geophysical surveys for the following parameters:

- *Gamma Log* Measures natural presence of gamma rays. Aids in defining lithology changes, bed boundaries and clay content.
- *Neutron Log* Measures the amount of hydrogen around the probe. Can provide an indication of porosity and clay content (in combination with gamma).
- Density (or gamma-gamma) Log Gamma source and gamma receiver measures the electron density, which is a function of the bulk density of the formation. This can also be used for fracture identification in some instances.
- Induction (medium and deep) Log The induction tool uses electromagnetics to sense the conductivity (inverse of resistivity) of the adjacent formation. Comparisons between deep and medium results can indicate porosity.
- *Point Resistance (PR) Log* Changes between a downhole electrode and a reference surface electrode reflect changes in the formation resistivity. This can represent changes in porosity, water salinity, and fluid connectivity.
- Calliper Log Spring-loaded arms that press against the side of the hole can indicate well and casing integrity. It can also be used to identify fractures in the lithology intercepted by the well.

In addition to the standard geophysical surveys, the EM Flowmeter was used under ambient and pumped conditions to determine vertical flow within the wells at discrete intervals sealed by inflatable packers. An acoustic televiewer survey was also conducted to provide an orientated, visual indication of fracture distribution within each well.

4. RECHARGE ESTIMATION TECHNIQUES

4.1 INTRODUCTION

The observation wells at the Forreston, Fox Creek and Mylor investigation sites were completed with the installation of nested piezometers with screens at discrete depth intervals. These were to enable sampling for a suite of hydrochemical, isotopic and radiogenic tracers to investigate the apparent groundwater age, depth of circulation, vertical and horizontal flow rates, and sources of groundwater. Aquifer pump tests were also conducted to determine some of the physical characteristics of the aquifer systems.

4.2 PIEZOMETER INSTALLATION

At the Forreston site, two piezometer nests were installed in open 203 mm holes. At Fox Creek, the piezometers were installed in a 203 mm and a 254 mm hole. At Mylor, a single 203 mm hole was used. PVC casing of 50 mm diameter was used with 0.5 m slotted screens positioned at intervals determined by the geophysical and EM Flowmeter surveys (Table 4.1). Wells were packed with gravel at piezometer screen depths and cemented between depths to isolate the groundwater flow to each piezometer. A full description of the lithological logs is provided in Appendix B.

4.3 GROUNDWATER AGES AND DEPTH OF CIRCULATION

4.3.1 MAJOR CHEMISTRY AND ISOTOPES

Prior to sampling the groundwater, the static water level was measured from top of casing (TOC) using an electric water level probe. The piezometers were then purged using a 12-volt Supertwister® submersible pump for the low-flow shallow piezometers and a Grundfos-MP1 submersible pump for the deeper piezometers. A YSI® multi-parameter meter was used to monitor the physical parameters of pH, specific electrical conductivity (SEC), dissolved oxygen (DO), redox and temperature during purging. The meter was calibrated with known standards prior to use in the field. Samples were collected once the physical parameters had stabilised, indicating that the sample was representative of the section of the aquifer sampled. The total alkalinity (assumed to be HCO_3^- for the ranges of pH sampled) was also measured in the field using an HACH titration kit.

Major ion analysis was conducted on the groundwater samples that had been filtered through a 0.45 μ m membrane filter in the field. Cations (Na⁺, Mg²⁺, K⁺, Ca²⁺ and NH₄⁺) and trace elements were acidified with nitric acid (1% v/v HNO₃) to keep the ions in solution and analysed by Inductively Coupled Plasma Emission Spectrometry (ICP-ES). Anions (Cl⁻, Br⁻, SO₄²⁻ and NO₃⁻) were analysed by Ion Chromatography (IC). Samples were also collected and analysed for the stable isotopes of the water molecule (deuterium (δ^2 H) and oxygen-18 (δ^{18} O)).

Table 4.1Construction details of the shallow and nested piezometers at the Forreston, Fox
Creek and Mylor investigation sites. Reduced standing water level (RSWL) is an
average of three measurements made between January 2006 and February 2007.

Unit number	Easting	Northing	Sample name	Surface elevation (m AHD)	Piezometer depth from surface (m)	TOC (PVC) elevation (m AHD)	Screen interval from surface (m)	Average RSWL (m AHD)
6628-22357	308036.64	6147499.68	F1	370.63	18.00	371.64	15.0–18.0	358.01
6628-22356	308036.64	6147499.68	F2	370.63	24.00	371.64	21.0–24.0	358.02
6628-22352	308036.15	6147493.62	F3	371.20	27.00	371.26	24.0-27.0	358.02
6628-22355	308036.64	6147499.68	F4	370.63	33.00	371.64	30.0–33.0	358.02
6628-22354	308036.64	6147499.68	F5	370.63	38.00	371.64	35.0–38.0	358.01
6628-22351	308036.15	6147493.62	F6	371.20	56.00	371.26	52.0-56.0	358.01
6628-22350	308036.15	6147493.62	F7	371.20	64.00	371.26	61.0–64.0	358.01
662822349	308036.15	6147493.62	F8	371.20	76.00	371.25	72.0–76.0	358.01
6628-22478	302579.86	6139401.96	L1	351.99	16.10	352.68	13.1–16.1	352.18
6628-22486	302579.86	6139401.96	L2	351.99	21.00	352.68	18.5–20.5	352.22
6628-22485	302579.86	6139401.96	L3	351.99	25.50	352.67	22.5–25.0	
6628-22481	302581.97	6139406.91	L4	351.83	28.50	352.29	25.0–28.0	352.22
6628-22484	302579.86	6139401.96	L5	351.99	30.50	352.68	27.0–30.0	352.23
6628-22483	302579.86	6139401.96	L6	351.99	34.50	352.67	32.0–34.0	352.24
6628-22482	302579.86	6139401.96	L7	351.99	38.50	352.68	36.0–38.0	352.24
6628-22480	302581.97	6139406.91	L8	351.83	40.50	352.30	37.0–40.0	352.23
6628-22479	302581.97	6139406.91	L9	351.83	51.50	352.29	47.0–51.0	352.26
6628-22478	302581.97	6139406.91	L10	351.83	62.50	352.29	56.0-62.0	352.27
6627-11286	295657.38	6120312.09	M1	308.02	16.00	308.88	10.0–16.0	303.23
6627-11285	295657.38	6120312.09	M2	308.02	30.00	308.88	24.0-30.0	303.24
6627-11284	295657.38	6120312.09	М3	308.02	48.00	308.88	42.0-48.0	303.08
6627-11283	295657.38	6120312.09	M4	308.02	65.00	308.88	59.0-65.0	303.00

Adelaide is the closest rainfall station to the RTC and ORC with rainfall isotopic data provided by the International Atomic Energy Agency (IAEA) Global Network of Isotopes in Precipitation (GNIP) service. For this study only, complete annual data sets from the GNIP database were used to derive the weighted average precipitation and the local meteoric water line (LMWL) for Adelaide (δ^2 H = 7.7, δ^{18} O = 9.9).

4.3.2 CARBON-14 AND CHLOROFLUOROCARBONS

Groundwater samples were collected for analysis of chlorofluorocarbons (CFCs), carbon-14 (¹⁴C) and dissolved inorganic carbon (δ^{13} C) to determine the apparent age of the water, and to provide information on the groundwater flow processes, including depth of circulation and vertical aquifer connection.

CFCs are stable organic compounds that were first manufactured in the 1930s and are produced solely from anthropogenic sources. Concentrations of CFCs in water vary as a

function of the atmospheric partial pressures of CFCs and CFC solubility (which is a function of salinity and temperature), and can be used to determine apparent groundwater age. CFCs can be measured in groundwater that has been recharged since ~1940, or in a mixture of groundwater younger than 1940 with older waters. CFCs have been used as age indicators for groundwater studies since ~1979 (Szabo et al. 1996).

Processes that affect the CFC age include sorption, contamination, microbial degradation, hydrodynamic dispersion and soil gas diffusion in the unsaturated zone. Corresponding errors in apparent CFC ages are $\sim \pm 2$ years for ages less than 20 years, increasing to ± 4 years for ages of 30 years. The detection limit for CFCs is ~ 5 pg/kg, which equates to an age of ~ 1961 (Leaney 2006).

Analysis of ¹⁴C can be used to support the CFC data and provide information for the older groundwaters that are beyond the capacity of the CFC dating technique. For a radioactive environmental tracer, where radioactive decay is the dominant process causing change in activity and the input activity of the tracer is relatively constant, then the groundwater age (*t*) can derived by:

$$t = -\lambda^{-1} \ln \left(\frac{A}{A_o}\right)$$
 Equation

where λ is the decay constant [T⁻¹], *A* is the measured activity and *A*_o is the estimated initial activity. (In this, and the following equations, L is length, T is time, M is mass.)

One of the complications with interpretation of ¹⁴C data is using an appropriate correction model to account for geochemical interactions that modify the initial activity (A_o) of ¹⁴C at the time of recharge. The correction models include a chemical mixing model (Tamers 1967), isotopic dilution model (Pearson & Hanshaw 1970) and a complete soil gas exchange model (Fontes & Garnier 1979). Required inputs for the models include the chemical and isotopic end members of soil gas δ^{13} C and ¹⁴C, partial pressure of CO₂ (pCO₂), and δ^{13} C and ¹⁴C of carbonates. These can be measured from samples in the laboratory and also approximated using the computer code PHREEQC (Parkhurst & Appelo 1999). The values used in this investigation are as follows: for initial activity (A_o) of soil CO₂ ¹⁴C = 85 pmC, soil gas δ^{13} C = -13‰, carbonate mineral δ^{13} C = -7.8‰ and carbonate mineral ¹⁴C = 0 pmC (Harrington 1999).

4.4 VERTICAL FLOW RATES AND AQUIFER RECHARGE

4.4.1 CARBON-14 AND CHLOROFLUOROCARBONS

Vertical profiles of groundwater age have been used successfully to estimate rates of vertical groundwater flow in sedimentary aquifers (Cook & Bohlke 1999). Assuming that sampling takes place near the watertable, then the horizontal component of groundwater flow will be relatively small and the recharge rate (R) may be approximated by:

$$R = \frac{z\theta}{t}$$
 Equation 4.2

where z is the depth below the watertable [L], t is the groundwater age [T] and θ is the porosity [unitless].

4.1

There are relatively few established and reliable techniques for estimating vertical flow rates in FRA (Love et al. 2002). One approach for determining vertical flow rates, and hence recharge rates, in an FRA assumes that groundwater flow occurs through vertical, planar, parallel fractures with uniform matrix properties. This assumption also implies a vertical distribution of groundwater ages. It is therefore necessary to have knowledge of various aquifer parameters including fracture aperture, which is determined from aquifer tests, fracture spacing (from fracture mapping), and estimates of the matrix diffusion coefficient. Where fracture orientations and distribution are more complex, groundwater ages are more likely to represent depth of groundwater circulation than provide information on vertical flow rates (Love et al. 2002).

For a conservative tracer with a constant source and subject to radioactive decay, the concentrations within the fractures can be related to vertical flow within the fractures (V_w) by:

$$V_{w} = \left[1 + \frac{\theta_{m} D^{\frac{1}{2}}}{b \lambda^{\frac{1}{2}}} \tanh(BD^{-\frac{1}{2}} \lambda^{\frac{1}{2}})\right] / \left[\frac{\delta t_{a}}{\delta z}\right]$$
 Equation 4.3

(after Neretnieks 1981)

where V_w is the groundwater velocity in the fracture $[LT^{-1}]$, *b* is the fracture half-aperture [L], *B* is the fracture half-spacing [L], θ_m is the matrix porosity [unitless], *D* is the effective diffusion coefficient within the matrix $[L^2T^{-1}]$, λ is the decay constant $[T^{-1}]$ and $\delta t_a/\delta z$ is the age gradient $[TL^{-1}]$. The decay constant for ¹⁴C is 1.21×10^{-4} /y. Cook and Simmons (2000) substituted the ¹⁴C decay constant with the exponential growth rate for CFC-12 (k = 0.06/y) to determine vertical flow rates from CFC-12 age gradients.

The mean volumetric flow rate through the fracture $(Q_v [L^3T^{-1}])$ is given by:

$$Q_v = V_w \frac{b}{B}$$
 Equation 4.4

4.4.2 AQUIFER PUMP TESTS

Single-well pump tests were conducted on several of the piezometers using the Cooper-Jacob straight-line method (Fetter 2001) to determine the bulk hydraulic conductivity over the length of the screen interval. Pump tests are typically more suited to sedimentary systems, but their application to nested piezometers can provide valuable information on the vertical variation of hydraulic conductivity and can be used to derive other physical characteristics of the aquifer (Cook 2003).

Having determined the bulk hydraulic conductivity over the screened interval from the aquifer tests, the average fracture aperture can be derived from:

 $K_b = \frac{\rho g(2b)^3}{12\mu(2B)}$ Equation 4.5

Rearranging equation 4.5, the equivalent fracture aperture can be determined:

 $2b_{eq} = \left(\frac{12\mu(2B)K_b}{\rho g}\right)^{1/3}$

Equation 4.6

where K_b is the bulk hydraulic conductivity over the test interval [LT⁻¹], *p* is the fluid density [ML⁻³], *g* is acceleration due to gravity [LT⁻²], 2*b* is the fracture aperture [L], μ is the dynamic viscosity [MT.L⁻¹] and 2*B* is the fracture spacing [L], which we have assumed to be the same as that in nearby outcrops of similar lithological type.

4.4.3 CHLORIDE MASS BALANCE

Groundwater recharge rates can also be estimated using the chloride mass balance (CMB) technique. The method assumes that the only source of chloride in groundwater is via rainfall and that the rate of chloride accession to the landscape is constant and there are no sources or sinks of chloride in the subsurface. The following steady state mass balance equation can be used to estimate recharge (R) by:

$$R = \frac{(P - RO)}{C_{gw}} C_p$$
 Equation 4.7

where *P* is the mean annual precipitation rate [L], *RO* is the annual runoff rate [L], C_p is the chloride concentration in the precipitation [ML⁻¹], and C_{gw} is the chloride concentration in groundwater [ML⁻¹].

The CMB technique has been used successfully in sedimentary aquifer systems and has been suggested as the most reliable technique for determining recharge rates to FRA systems (Cook 2003). However, the recharge rate determined from CMB should be considered as a minimum because of the addition of other sources of chloride. Changes in environmental conditions (i.e. vegetation clearing) will also impact on the equilibrium of chloride in the fractures with the rock matrix and may take a significant amount of time for the diffusion of salts from the matrix into the fractures to re-equilibrate.

4.5 HORIZONTAL FLOW VELOCITIES FROM RADON ACTIVITY

Radon (222 Rn) is a radioactive inert gas that is generated from the decay of uranium and thorium series isotopes in the aquifer matrix. It has a half-life of ~3.8 days, is highly soluble in water, and its concentration will depend on the mineralogy of the aquifer and the pore space geometry (Love et al. 2002).

Cook et al. (1999) developed a technique to estimate horizontal flow rates by comparing unpurged to purged ²²²Rn concentrations from piezometers, where a purged sample is assumed to be representative of the concentration of ²²²Rn in the aquifer. For high horizontal flow rates, the concentration of ²²²Rn of an unpurged sample, measured over the length of the screen of the piezometer, will be similar to the concentration of a purged sample from the piezometer. If the horizontal flow rate were low, then the concentration of ²²²Rn of an unpurged sample would have decayed to background levels. Hence, the ratio of ²²²Rn concentration from an unpurged sample to a purged sample will depend on the amount of radioactive decay, which occurs as the groundwater moves through the well under natural flow conditions. Assuming a perfectly mixed well, the groundwater flow rate (*q*, m/y) is given by:

$$q = \frac{c}{c_0 - c} \frac{\lambda \pi r}{2}$$

Equation 4.8

where *c* and *c*₀ are the ²²²Rn concentrations (Bq/L) in the well and in the aquifer respectively, *r* is the well radius (m) and λ is the decay constant for ²²²Rn (0.18/d). Groundwater flow rates calculated by this method refer to groundwater flow within the well. Due to hydrodynamic dispersion, the horizontal flow rate within the well will be higher than in the aquifer. To estimate flow within the aquifer, the calculated flow rate needs to be multiplied by a factor of 0.5 for an open well or 0.25 for a piezometer.

5. FIELD INVESTIGATIONS

5.1 FORRESTON INVESTIGATION SITE

The Forreston investigation site is located in the north of the RTC at an elevation of \sim 380 m AHD in an area of moderately steep topography and with an annual rainfall of \sim 800 mm.

Piezometer nests were installed in two 203 mm holes, with depths of 43 and 80.4 m, referred to below as Fr1 and Fr2, respectively. Surface casing was installed to 4.4 m in Fr1 and to 3.1 m in Fr2. These two holes were completed as nested piezometers as detailed in Table 4.1 (piezometers F1 to F8). The site is situated in the Woolshed Flat Shale; detailed lithological logs are included in Appendix B.

5.1.1 FRACTURE ANALYSIS

Detailed fracture analyses were undertaken at two locations in close proximity to the Forreston investigation site to provide values of fracture spacing for use in the parallel-plate model.

Field measurements indicate the dominant fracture set has an orientation of $002^{\circ}/67^{\circ}E$. This is represented diagrammatically by the stereographic projection of poles to fracture surfaces in Figure 5.1. The great circle girdles represent the average fracture orientation (black) and outcrop-scale bedding (green), indicating that the dominant fracture set is parallel to the regional cleavage orientation (S₁ 002°/66°E). On a macroscopic scale, the dominant fracture set is also sub-parallel to bedding (S₀ 002°/70°E). Average spacing between parallel fracture surfaces is 13 mm, and frequency analysis indicates that 86% of fracture spacings lie within the 0–20 mm range (Fig. 5.2).

5.1.2 ELECTRICAL CONDUCTIVITY, TEMPERATURE AND PH IN OPEN WELLS

EC, temperature and pH were measured using a $YSI^{\$}$ 600XL Series Sonde for the open 203 mm holes (Fig. 5.3). The sonde recorded these variables from the watertable, at ~11.5 m depth in both holes, to 44 m (TOC) in Fr1 and to a depth of 80.4 m (TOC) in Fr2.

These measurements in the two wells show distinctly different results. The EC in Fr1 is uniform at ~750 μ S/cm for the whole measured depth. There was more variation in Fr2, with a steady decrease from 835 μ S/cm at 2 m below the watertable to ~786 μ S/cm at 30 m depth, then remaining constant down to a depth of 79 m. Below 79 m there is a marked increase in EC down to the 80.2 m limit of the measurements. This EC increase corresponds to an increase in pH at the same depth and may indicate inflow from a significant fracture at that depth.



Figure 5.1 Lower Hemisphere Equal Area Stereographic Projection of fracture sets at the Forreston investigation site (n = 410)



Figure 5.2 Frequency plot of fracture spacings measured over a 2 m interval (n = 160) at the Forreston investigation site



Figure 5.3 EC, temperature and pH variation with depth in the 203 mm open holes (Fr1 and Fr2) at the Forreston investigation site, August 2005. Both holes are cased to ~6 m. Fr1 and Fr2 are 42 and 80 m deep, respectively.

The temperature in Fr1 decreases along a constant gradient from 17.5° C at the watertable to 14.1°C at 44 m depth. In Fr2 there is a slight but steady increase in temperature with depth from 17.5° C at the watertable to 18.1° C at 80 m depth. The pH in Fr1 increases along a constant gradient from 6.70 at the watertable to 7.76 at 44 m depth. The pH in Fr2 declines from 7.21 at the watertable to 6.74 at ~32 m depth, then remains fairly constant, decreasing by only 0.12 to 6.62 at 79 m depth, prior to a marked increase to 6.92 at 80.4 m.

5.1.3 GEOPHYSICAL AND EM FLOWMETER SURVEYS IN OPEN WELLS

Calliper and EM Flowmeter results (Fig. 5.4) are used to aid in the identification of strata changes and identify the principle flow zones to determine where the nested piezometer screen intervals should be located.

Deviations in the calliper trace, such as seen at \sim 21 and 23 m for Fr1, and at 25 and 32 m for Fr2, indicate positions where the holes intersect significant fractures.



Figure 5.4 Calliper (a) and EM Flowmeter (b) profiles in the 203 mm hole Fr1 (~44 m) and calliper (c) and EM Flowmeter (d) profiles in the 203 mm hole Fr2 (~80 m) at the Forreston investigation site, August 2005. Water level at time of measurement was ~10 m below surface. Diamonds on the flowmeter profile represent intervals where the packers were inflated to measure flow. Both holes are PVC cased to 6 m.

The EM Flowmeter results suggest that there is a small amount (1.5 L/min) of upward flow at \sim 23 m depth in Fr1. This corresponds with a spike in the calliper trace, which may indicate a fracture at this depth. Apart from this, EM Flowmeter results for both holes display very little flow under ambient conditions.

5.1.4 HYDRAULICS

The average watertable elevations measured in January and April 2006 in the nested piezometers are shown in Figure 5.5. The primary y-axis shows the piezometer screen elevation, whilst the secondary y-axis shows the watertable elevation corrected to an RSWL in each of the piezometers. There is no significant difference in groundwater head between the shallow and deep piezometers. Hence, there is no hydraulic gradient over the depth range of these piezometers and, as shown in the EM Flowmeter profile (Fig. 5.4), no ambient vertical flow across this range.





5.1.5 AQUIFER PUMP TESTS

Attempts to maintain a drawdown of water level over a 100-minute pump test were unsuccessful at the Forreston site because of the high yield of the FRA. In all of the piezometers, pumping from the depth of the screen interval at a rate of ~18 L/min resulted in a stabilised drawdown of only a few centimetres within 2–3 minutes. These results indicate that at this location there is a fairly high conductivity at all of the piezometer screen depths.

The Cooper-Jacobs straight-line method, which requires the monitoring of continuous drawdown over a longer period, could not be applied to determine hydraulic conductivity values in this case. Instead, the final drawdown and the applied pumping rate were used in a Darcy's law calculation to approximate the bulk conductivity (Kb) at the depths of four of the piezometer screens. Fracture aperture values (*2b*) were then calculated for these four depths using equation 4.2 (section 4.4). The calculated values of Kb and *2b* are highlighted in yellow in Table 5.1.

Piezo- meter interval	Screen length	Aquifer test bulk K Kb	Fracture spacing 2B	Hydraulic gradient dh/dx	Fluid density ρ	Gravity g	Dynamic viscosity μ	Fracture aperture 2b	Fracture aperture 2b
	(m)	(m/d)	(m)		(kg/m ³)	(m/s ²)	(kg/s/m)	(m)	(μ m)
F2	3.0	15.9 *	0.013	0.007	1000	9.8	0.00114	1.495E-04	149
F5	3.0	4.1 *	0.013	0.007	1000	9.8	0.00114	9.513E-05	95
F6	4.0	3.7 *	0.013	0.007	1000	9.8	0.00114	9.193E-05	92
F7	3.0	2.1 *	0.013	0.007	1000	9.8	0.00114	7.611E-05	76

Table 5.1Aquifer properties determined from aquifer pumping tests and observations in four
piezometers at the Forreston investigation site

* bulk K values determined from Darcy's Law approximation.

5.2 FOX CREEK INVESTIGATION SITE

The Fox Creek investigation site is located on Fox Creek Road, ~5 km northwest of Lobethal, in an area of steeply incised valleys at an elevation of ~360 m AHD. Annual rainfall here is ~840 mm.

Piezometer nests were installed in a 254 mm hole of 40.29 m depth and an 203 mm hole of 90.60 m depth, referred to below as FC1 and FC2, respectively. Surface casing for FC1 was installed to 10.5 m, and to 14 m in FC2. These two holes were completed as nested piezometers as detailed in Table 4.1 (piezometers L1 to L10). The lithology encountered during drilling was slate of the Saddleworth Formation. Lithological logs for the two holes are provided in Appendix B.

5.2.1 FRACTURE ANALYSIS

Detailed fracture analyses were undertaken at the Fox Creek investigation site to provide values of fracture spacing for use in the parallel-plate model.

Field measurements indicate that the dominant fracture set has an orientation of $002^{\circ}/46^{\circ}E$. This is represented diagrammatically by the stereographic projection of poles to fracture surfaces in Figure 5.6. The great circle girdles represent the average fracture orientation (black) and outcrop-scale bedding (green), indicating that the dominant fracture set is sub-parallel to the bedding orientation (S_o $024^{\circ}/43^{\circ}E$). The blue great circle girdle represents the cleavage orientation (S₁ $010^{\circ}/55^{\circ}W$).

Average spacing between parallel fracture surfaces is 14 mm, and frequency analysis indicates that 87% of fracture spacings lie within the 0–20 mm range (Fig. 5.7).



Figure 5.6 Lower Hemisphere Equal Area Stereographic Projection of fracture sets at the Fox Creek investigation site (n = 150)



Figure 5.7 Frequency plot of fracture spacings measured over a 0.5 m interval (n = 15) at the Fox Creek investigation site

5.2.2 EC, TEMPERATURE AND PH IN OPEN WELLS

EC, temperature and pH were measured using a $YSI^{\$}$ 600XL Series Sonde for the open 254 mm hole (FC1) from the watertable, at ~0.7 m, to a depth of 40.29 m (TOC) (Fig. 5.8).

The EC in FC1 is uniform at ~1400 μ S/cm for the whole measured depth, which suggests a good connection between fractures over the entire 40 m depth. The temperature in FC1


Figure 5.8 EC, temperature and pH variation with depth in the 40.3 m deep 254 mm open hole (FC1) at the Fox Creek investigation site, November 2005

increases slightly with depth, from 15.5° C at the watertable to 16.5° C at 40 m depth. The pH increases from 6.80 at the watertable to 7.50 at ~20 m depth, and then remains approximately constant down to 40 m depth.

5.2.3 GEOPHYSICAL AND EM FLOWMETER SURVEYS IN OPEN WELLS

Deviations in the calliper trace indicate positions where the hole intersects significant fractures. The greatest deviations in the FC1 calliper trace (Fig. 5.9a) are at ~20 and 34 m; significant deviations are also seen between 11-27 m, and at 27.5 m. In the FC2 calliper trace (Fig. 5.9c), several major deviations are seen between depths of 30 and 50 m, while smaller deviations are also seen between 14-16 m and at 22 m.





The EM Flowmeter trace for FC1 suggests that under pumped conditions, nearly all of the flow into the hole originates from a depth between 29–32 m. This does not correspond to any of the major deviations in the calliper trace for this hole, but suggests that there is a fracture at that depth that is able to conduct a large volume of groundwater. The EM Flowmeter traces for FC1 display very little flow under ambient conditions.

The EM Flowmeter trace for FC2 shows an upward flow of up to 4 L/min under ambient conditions. The flow is greatest between 30–45 m depth, and declines toward the top of the hole. The greater flow corresponds with the location of the largest deviation in the calliper trace, suggesting flow into the hole through fractures at these depths, and flow out of the hole via fractures above 20 m depth. Under pumped conditions, with 10 L/min pumped from near the top of the hole, upward flow is seen to increase significantly between 45–30 m depths, but with no further increase above 30 m. This indicates that the majority of the flow into the hole is via the larger fractures below 30 m depth.

5.2.4 HYDRAULICS

The average watertable elevations measured in September and October 2006 in the nested piezometers are shown in Figure 5.10. The primary y-axis shows the piezometer screen elevation, whilst the secondary y-axis shows the watertable elevation corrected to an RSWL in each of the piezometers. There is a head difference of 0.1 m between the deepest and shallowest piezometers at this site, with the highest head elevations at greater depth, creating a positive (upward) hydraulic gradient. The hydraulic gradient in FC1, from 14.6–37 m, is ~0.0022 (0.05 m/22.4 m). In FC2, the hydraulic gradient is 0.0015 (0.05 m/32.5 m) between 59.0–26.5 m depth. These upward gradients help to explain the upward flows identified in FC2, as water flows into the well from the larger fractures near the bottom of the hole, and flows out via fractures near the top of the well.

5.2.4 AQUIFER PUMPING TESTS

The required 100-minute aquifer pumping tests were successfully completed in four piezometers (L1, L5, L8 and L10). The bulk hydraulic conductivity (Kb) values resulting from application of the Cooper-Jacobs straight-line method to the results of these tests are shown in Table 5.2. For piezometers in which a pumping test was not conducted, averages of the drawdown log cycle in the adjacent depths were used to provide a K value. Fracture aperture (*2b*) values were also calculated for these four depths using equation 4.2 (section 4.4).

There was considerable drawdown of up to 9.5 m in the shallowest piezometer with a pumping rate of only 4–5 L/min, indicating a low yield and poorly connected fractures at that depth. Yields were higher in deeper piezometers, with drawdowns of ~1 m at pumping rates of ~10 L/min.

The pumping tests at this site also indicated very strong connectivity between the two wells, and over a range of depths. When any of the piezometers were pumped, a similar drawdown occurred in adjacent piezometers.

5.3 MYLOR INVESTIGATION SITE

The Mylor investigation site is located on Stock Road \sim 3 km south of Mylor. This is an area of moderately steep topography at an elevation of \sim 310 m AHD and with an annual rainfall of \sim 840 mm.

Piezometer nests were installed in a single 203 mm hole of 80.1 m depth. Surface casing was installed to a depth of 10 m. The hole was completed with four nested piezometers (M1–M4) as detailed in Table 4.1. The lithology encountered during drilling was Aldgate Sandstone. Lithological logs for this hole are provided in Appendix B.

FIELD INVESTIGATIONS

Piezometer interval	Screen length	Drawdown log cycle h₀-h	Flow rate	Constant discharge rate Q	Transmissivity (Cooper- Jacobs) T	Aquifer test bulk K Kb	Fracture spacing 2B	Hydraulic gradient dh/dx	Fluid density ρ	Gravity g	Dynamic viscosity μ	Fracture aperture 2b	Fracture aperture 2b
	(m)	(m)	(L/min)	(m ³ /d)	(m²/d)	(m/d)	(m)		(kg/m ³)	(m/s ²)	(kg/s/m)	(m)	(μ m)
L1	3.0	6.5	5	7.2	0.203	0.068	0.08	0.007	1000	9.8	0.00114	4.436E-05	44
L2	2.0	0.27	4	5.76	3.905	1.952	0.08	0.007	1000	9.8	0.00114	1.361E-04	136
L4	3.0	0.6	10	14.4	4.393	1.464	0.08	0.007	1000	9.8	0.00114	1.237E-04	124
L5	3.0	0.6	10	14.4	4.393	1.464	0.08	0.007	1000	9.8	0.00114	1.237E-04	124
L6	2.0	0.605	10	14.4	4.356	2.178	0.08	0.007	1000	9.8	0.00114	1.412E-04	141
L7	2.0	0.415	10	14.4	6.351	3.175	0.08	0.007	1000	9.8	0.00114	1.601E-04	160
L8	3.0	0.41	10	14.4	6.428	2.143	0.08	0.007	1000	9.8	0.00114	1.404E-04	140
L9	4.0	0.4	10	14.4	6.589	1.647	0.08	0.007	1000	9.8	0.00114	1.286E-04	129
L10	6.0	0.405	10	14.4	6.508	1.085	0.08	0.007	1000	9.8	0.00114	1.119E-04	112

 Table 5.2
 Aquifer properties determined from aquifer pumping tests and observations at the Fox Creek investigation site. Calculated values of bulk hydraulic conductivity (Kb) and average fracture aperture (2b) are highlighted in yellow



Figure 5.10 Average watertable elevations in the nested piezometers at the Fox Creek investigation site. RSWL averaged from two measurements taken in September and October 2006 are shown against a scale of m AHD on the right-hand axis. Piezometer screen depths are plotted on a scale of m AHD on the left-hand vertical axis.

5.3.1 FRACTURE ANALYSIS

Detailed fracture analyses were undertaken at two locations in close proximity to the Mylor investigation site to provide values of fracture spacing for use in the parallel-plate model.

Field measurements indicate that the dominant fracture set has an orientation of 003°/89°E. This is represented diagrammatically by the stereographic projection of poles to fracture surfaces (Fig. 5.11). The great circle girdles represent the average fracture orientation (black) and regional cleavage (blue), indicating that the dominant fracture set is parallel to





the regional cleavage orientation (S₁ 002°/90°). The green great circle represents macroscopic scale bedding (S₀ 041°/18°E). In addition to the dominant cleavage-parallel fracture set, a number of significant fracture sets are also illustrated by the contoured stereographic projection, orientated 046°/77°E, 041°/17°E, 046°/52°W and 160°/82°E.

Average spacing between fracture surfaces for the dominant cleavage parallel fracture set is 95 mm, and frequency analysis indicates that 92% of fracture spacings lie within the 0–200 mm range (Fig. 5.12).



Figure 5.12 Frequency plot of fracture spacings measured over a 1 m interval (n=12) at the Mylor investigation site

5.3.2 EC, TEMPERATURE AND PH IN OPEN WELLS

EC, temperature and pH were measured using a YSI^{\otimes} 600XL Series Sonde for the open 203 mm hole (Fig. 5.13). The sonde recorded these variables from the watertable, at ~1.40 m depth (TOC), to a depth of 80.4 m (TOC).

There is a distinct change in EC and temperature in the upper 5 m of the well, and in pH in the upper 10 m. However, these variations are probably due only to temperature equilibration of the sonde in the first few minutes of measurement, and effects of standing water in the well casing in the upper 10 m of the well. The variation in EC toward the bottom of the well is more significant. The reduction in EC from \sim 60–66 m, and increase in EC from 73–80 m, may indicate inflows of groundwater into the hole at these depths.



Figure 5.13 EC, temperature and pH variation with depth in the 80.1 m deep 203 mm open hole at the Mylor investigation site, December 2005

5.3.3 GEOPHYSICAL AND EM FLOWMETER SURVEYS IN OPEN WELL

Deviations in the calliper trace indicate positions where the hole intersects significant fractures. The greatest deviation in the calliper trace for the Mylor 203 mm hole is seen between ~10–20 m (Fig. 5.14). In this case however, the calliper deviation is indicative of a collapse of the side of the hole between these depths, increasing the overall diameter of the hole to up to 275 mm at ~18 m depth. Significant deviations are also seen between 38–48 m, with some smaller deviations apparent between 25–34 m.

The EM Flowmeter trace for FC1 suggests that under ambient conditions there is a small upward flow of 1.5 L/min from the bottom to the top of the well. When pumping 3 L/min from 2.35 m depth, nearly all of the additional flow into the well originates from a depth between 30–34 m, with the remainder entering the well between 10–22 m depth, indicating the presence of conductive fractures within these depth ranges.



Figure 5.14 Calliper (a) and EM Flowmeter (b) profiles in the 203 mm open hole at the Mylor investigation site in May 2005. Water level at time of measurement was ~1.25 m below surface. Diamonds on the flowmeter profile represent intervals where the packers were inflated to measure flow. The hole is PVC cased to a depth of 10 m.

5.3.4 HYDRAULICS

The average watertable elevations measured in September and November 2006 in the nested piezometers are shown in Figure 5.15. The primary y-axis shows the piezometer screen elevation, whilst the secondary y-axis shows the watertable elevation corrected to an RSWL in each of the piezometers. There is a head difference of 3 m between the deepest and shallowest piezometers at this site, with the highest head elevations at greater depth, creating a strong positive (upward) hydraulic gradient. The hydraulic gradient from 13–62 m is ~0.061 (3.00 m/49.0 m). This upward gradient explains the upward flows identified by the EM Flowmeter, as groundwater flows into the hole from near the bottom of the well, and flows out via fractures near the top of the well. Although there is a strong hydraulic gradient, the rate of ambient flow is low at ~1.5 L/min, suggesting that the fractures intersected by the well have a relatively low conductivity.

5.3.5 AQUIFER PUMPING TESTS

Aquifer pumping tests were successfully completed in all four piezometers at the Mylor investigation site. The bulk hydraulic conductivity (Kb) values were calculated by application of the Cooper-Jacobs straight-line method to the results of these tests. Fracture aperture (*2b*) values were also calculated for these four depths using equation 4.2 (section 4.4). The calculated values of Kb and *2b* are highlighted in yellow in Table 5.3.

There was considerable drawdown of between 4–18 m in these piezometers with a pumping rate of only 1 L/min, indicating a very low yield and poorly connected fractures at all depths.

The pumping tests also showed very poor connectivity between piezometers. When any of the piezometers were pumped there was no measurable drawdown in the other piezometers, even with very high drawdown in the pumped piezometer.



Figure 5.15 Average watertable elevations in the nested piezometers at the Mylor investigation site. The RSWL averaged from two measurements taken in September and November 2006 are shown against a scale of m AHD on the righthand axis. Piezometer screen depths are plotted on a scale of m AHD on the left-hand vertical axis.

FIELD INVESTIGATIONS

Piezometer interval	Screen length	Drawdown log cycle h₀-h	Flow rate	Constant discharge rate Q	Transmissivity (Cooper- Jacobs) T	Aquifer test bulk K Kb	Fracture spacing 2B	Hydraulic gradient dh/dx	Fluid density ρ	Gravity g	Dynamic viscosity μ	Fracture aperture 2b	Fracture aperture 2b
	(m)	(m)	(L/min)	(m ³ /d)	(m²/d)	(m/d)	(m)		(kg/m ³)	(m/s ²)	(kg/s/m)	(m)	(µ m)
M1	6.0	2.465	1.1	1.584	0.118	0.020	0.1	0.007	1000	9.8	0.00114	3.163E-05	32
M2	6.0	14.02	0.6	0.864	0.011	0.002	0.1	0.007	1000	9.8	0.00114	1.448E-05	14
M3	6.0	6.67	1.1	1.584	0.043	0.007	0.1	0.007	1000	9.8	0.00114	2.270E-05	23
M4	6.0	9.7	0.85	1.224	0.023	0.004	0.1	0.007	1000	9.8	0.00114	1.839E-05	18

Table 5.3 Aquifer properties determined from aquifer pumping tests and observations at the Mylor investigation site

6. GROUNDWATER AGES AND DEPTH OF CIRCULATION

This chapter provides an examination and interpretation of the data sets that were used to establish a conceptual model of groundwater recharge mechanisms, vertical circulation and sources to the aquifer systems at the Forreston, Fox Creek and Mylor investigation sites.

6.1 FORRESTON INVESTIGATION SITE

6.1.1 MAJOR CHEMISTRY AND ISOTOPES

Figure 6.1 shows the measured total dissolved solids (TDS), chloride (Cl⁻), deuterium (δ^2 H) and pH profiles with depth at the Forreston investigation site. There is little change in either TDS or Cl⁻ with depth, both increasing by ~20% between the shallowest piezometer at 16.5 m and the deepest at 74 m. The similarity between the Cl⁻ and TDS depth profiles suggests that there is minimal change in hydrochemical composition with depth. There is no clear trend in changes of pH with depth.

There are some variations in δ^2 H ratio with depth, but these are not reflected in changes in Cl⁻ or TDS concentrations, which would occur if the δ^2 H changes were a result of different degrees of evaporation prior to recharge. The variations in δ^2 H with depth are therefore interpreted to be a result of long-term periodic differences in rainfall δ^2 H over time at this location.

Chloride generally does not participate in common geochemical reactions that occur in aquifers and subsequently behaves as a conservative tracer until saturation is reached (Herczeg & Edmunds 1999). Rainwater in near-coastal areas typically has a major ion composition with the same proportions of the major ions as found in seawater.



Figure 6.1 TDS, Cl⁻, δ^2 H and pH profiles sampled at the Forreston investigation site, January–February 2006. The depth shown for each data point represents the midpoint of the 3 m piezometer screen interval.

If the observed changes in groundwater TDS concentrations with depth are solely a result of evaporation prior to recharge, we should expect to see the changes in all of the major inorganic ions remain in the same proportion relative to Cl⁻ as they are in the rainwater in the locale of the aquifer recharge. As the dissolved salts in near-coastal rainwater are derived from marine aerosols, the ratios of the major ions in rainwater are expected to be similar to those in seawater. Figure 6.2 shows the concentrations of major ions (Ca²⁺, Mg²⁺, Na⁺, K⁺, SO₄²⁻ and HCO₃⁻) against Cl⁻ and their proximity to the respective seawater ion/Cl⁻ relationship. All the Forreston samples are closely grouped and plot well above the seawater ion/Cl⁻ ratio in each ion/Cl⁻ graph. This pattern suggests dissolution of ions as a result of interactions with soil or rock during or after recharge. The concentration, implying that rainwater Cl⁻ concentrations have not been affected by these water–rock interactions. The HCO₃⁻ concentration is much higher than the other major ions relative to the seawater ratio, and this may be explained by dissolution of CO₂ as the water passes through soil prior to recharging groundwater.

In all of these graphs, the groundwater from greater depths tends to plot further along the X and Y-axis, reflecting the slightly higher TDS at greater depth, as seen in Figure 6.2.

The most striking feature of the plots of the major cations against Cl⁻ is the close grouping of all the groundwater samples from the Forreston site, indicating that groundwater at all depths appears to have undergone similar processes during and after recharge, suggesting strong hydrologic connection and a common recharge zone and flow path for the groundwater at all depths.

6.1.2 CARBON-14 AND CHLOROFLUOROCARBONS

The CFC-12 concentrations indicate relative groundwater ages. All of the CFC-12 concentrations of samples from the Forreston site were much greater than the present-day concentration of 240 pg/kg (Fig. 6.3) indicating contamination of these samples from a CFC-12 source other than atmospheric CFCs. Duplicate samples taken from this site in April 2006 were found to have similar CFC-12 concentrations to the January 2006 samples, confirming that the groundwater at this location is contaminated by a concentrated source of CFC-12. Although this source cannot be identified without further investigation, the CFC-12 concentrations appear to decrease with depth, suggesting dispersion from a source near the surface. While this contamination precludes the possibility of using CFC-12 concentrations for groundwater age dating at this site, the presence of CFC-12 at the deepest piezometer indicates that if the contamination source is near the surface, groundwater has reached that depth (76 m) since recharging at a time later than the introduction of CFC-12 in manufactured products in 1965. As illustrated by the data in Table 6.1, the presence of modern groundwater at all depths is also supported by the high ¹⁴C activities (92.2–98.7 pmC). Values of groundwater ¹⁴C activity (denoted as 'A' in Table 6.1) above 90 pmC are taken to be affected by post-1950 radiogenic ¹⁴C. Hence, both the CFC-12 concentrations and ¹⁴C activities suggest that groundwater at all depths sampled at this site has recharged within the last 50 years.



Figure 6.2 Composition diagrams of major ions versus CI⁻ sampled at the Forreston investigation site, January–February 2006. The dashed line is the dilution line for the respective ion/CI⁻ ratio in seawater. Piezometer mid-screen depths are shown beside each point.



- Figure 6.3 Depth profile of CFC-12 concentrations (a) and ¹⁴C activities (b) of groundwater from the nested piezometers at the Forreston investigation site. The average watertable depth was 12.9 m below surface in January 2006 when sampling was completed. The error bars represent the piezometer screen length from which the sample was taken.
- Table 6.1 Uncorrected and corrected ¹⁴C ages for samples from the Forreston investigation site. Corrected ages are derived using the Fontes and Garnier (1979) correction model. Data on the sample δ^{13} C and HCO₃, and CO₂ molar concentrations are used in the correction model. The values of both the δ^{13} C and ¹⁴C activities of the FRA carbonates and soil CO₂ are also used in the correction model. Values used here were: $\delta^{13}C_{carbonate} = -7.8^{\circ}/_{oo}, \delta^{13}C_{soilCO2} = -13^{\circ}/_{oo}, A_{carbonate} = 0 \text{ pmC}, A_{soilCO2} = 85 \text{ pmC}.$

Sample	Depth	A (pmC)	δ ¹³ C	НСО 3 (m)	CO ₂ (m)	Uncorrected age (y)	Corrected age [F & G model] (y)
F1	16.5	94.25	-19.10	0.00290	0.00290	-592	969
F2	22.5	93.29	-17.90	0.00298	0.00298	-533	117
F3	25.5	97.10	-16.20	0.00290	0.00290	-763	-1 717
F4	31.5	98.70	-18.20	0.00314	0.00314	-856	35
F5	36.5	94.40	-17.20	0.00292	0.00292	-601	-558
F6	54.0	92.17	-17.10	0.00330	0.00330	-464	-514
F7	61.0	92.40	-17.00	0.00317	0.00317	-478	-622
F8	74.0	90.81	-17.30	0.00314	0.00314	-379	-245

Because ¹⁴C activities above 90 pmC are considered to be affected by radiogenic carbon, the high ¹⁴C activities in these samples result in negative age values when used to derive an age for the groundwater samples (Table 6.1). Application of the Fontes and Garnier correction model to these values results in an inconsistent range of ages, which are not useful in understanding groundwater flow or recharge at this site. However, the high values are indicative of relatively young (<50 years) groundwater, suggesting a fairly high groundwater flow rate.

6.2 FOX CREEK INVESTIGATION SITE

6.2.1 MAJOR CHEMISTRY AND ISOTOPES

Figure 6.4 shows the measured TDS, Cl⁻, δ^2 H and pH profiles with depth at the Fox Creek investigation site. There is little change in either TDS or Cl⁻ with depth. The Cl⁻ concentration increases by ~19% between the shallowest piezometer at 14.6 m and the deepest at 59 m, while TDS increases by ~4% across this depth range. The similarity between the Cl⁻ and TDS depth profiles suggests that there is minimal change in hydrochemical composition with depth. There is no clear trend in changes of pH with depth.

There are some variations in δ^2 H ratio with depth. The δ^2 H values appear to fall into two distinct groups, with more enriched values in the shallower part of the system and more depleted values in the deeper part. These differences are not reflected in changes in Cl⁻ or TDS concentrations, which would be expected if the δ^2 H changes were a result of different degrees of evaporation prior to recharge. Aquifer pumping tests have indicated that there is good connection between all piezometers at this site. The variations in δ^2 H with depth are therefore interpreted to be a result of periodic differences in rainfall δ^2 H over time at this location.



Figure 6.4 TDS, Cl⁻, δ^2 H, and pH profiles sampled at the Fox Creek investigation site, October 2006. The depth shown for each data point represents the mid-point of the 3 m piezometer screen interval.

Figure 6.5 shows the relationships of major ion $(Ca^{2+}, Mg^{2+}, Na^+, K^+, SO_4^{2-} and HCO_3^-)$ concentrations with the Cl⁻ concentration and their proximity to the respective seawater ion/Cl⁻relationship. Most of the ion/Cl⁻ ratios lie away from the seawater ion/Cl⁻ ratio, indicating that the hydrochemical composition is influenced by factors other than just evaporation and that groundwater at all sampled depths is influenced by water–rock interaction. There appear to be no trends in the position of samples from different depths in relation to the sea water dilution line in any of the graphs in Figure 6.5. The most striking feature of the plots is the close grouping of all the groundwater samples, indicating that groundwater at all depths appears to have undergone similar processes during and after recharge. This similarity in the chemical compositions probably reflects the strong hydrologic connection between depths observed in the aquifer pumping tests at this site and suggests a common recharge zone and flow path for the groundwater at all depths.

The ion/Cl⁻ relationships for Na⁺, K⁺, and Mg²⁺ lie close enough to the seawater dilution line to be solely a result of evaporative concentration of rainwater. The Ca²⁺/Cl⁻ and HCO₃⁻/Cl⁻ ratios are both elevated with respect to the seawater ratios and probably indicate dissolution of CaCO₃. However, whereas Ca²⁺ is elevated by ~0.6 mmol/L, HCO₃⁻ is elevated by ~4 mmol/L, which must be largely due to soil CO₂ dissolution prior to recharge. The SO₄²⁻/Cl⁻ ratio is ~0.4 mmol lower in SO₄²⁻ than the seawater ratio. This is probably a result of CaSO₄ precipitation resulting from higher Ca²⁺ concentration after dissolution of CaCO₃.

6.2.2 CARBON-14 AND CHLOROFLUOROCARBONS

The CFC-12 concentrations for the Fox Creek site (Fig. 6.6) are all low, with only the uppermost piezometer at 14.6 m having a concentration high enough to provide a definitive age of 38 years. Below that depth, the CFC-12 concentrations were sufficient only to show that the age of the groundwater is greater than 40 years.

The ¹⁴C activities at the Fox Creek site are all very low, indicating the groundwater here is quite old. Uncorrected ¹⁴C ages range from 7470 years at 14.6 m depth to 16 787 years at 59 m depth. When corrected according to the Tamers correction model (Table 6.2), which accounts for some carbonate dissolution (as identified in groundwater at this site in section 6.2.1), the ages range from 3569 years at 14.6 m depth to 12 926 years at 59 m depth.

The variation of 14 C age with depth (Fig. 6.7) provides a uniform age gradient throughout the range of piezometer depths at this site. Both uncorrected and corrected ages provide an age gradient of 204 y/m.

For the 14.6 m depth, there is clearly a conflict between the ¹⁴C age of 3569 years and the CFC-12 age of 38 years. The aquifer pumping tests showed that groundwater at this location was very strongly connected between all piezometer depths, so the consistent ¹⁴C age gradient between 14.6 m and all the deeper piezometers tends to support the credibility of the ¹⁴C age rather than the CFC-12 age for the 14.6 m sample.



Figure 6.5 Composition diagrams of major ions versus Cl⁻ sampled at the Fox Creek investigation site in October 2006. The dashed line is the dilution line for the respective ion/Cl⁻ ratio in seawater. Piezometer mid-screen depths are shown beside each point.







Figure 6.7 Depth profiles of ¹⁴C activities and ¹⁴C apparent ages from the piezometers at the Fox Creek investigation site, October 2006. The error bars represent the piezometer screen length from which the sample was taken.

Table 6.2 Uncorrected and corrected ¹⁴C ages for samples from the Fox Creek investigation site. Corrected ages are derived using the Tamers (1967) correction model. Data on the sample δ^{13} C and HCO₃, and CO₂ molar concentrations are used in the correction model. The values of both the δ^{13} C and ¹⁴C activities of the FRA carbonates and soil CO₂ are also used in the correction model. Values used here were: $\delta^{13}C_{carbonate} = -7.8^{\circ}/_{oo}$, $\delta^{13}C_{soilCO2} = -13^{\circ}/_{oo}$, $A_{carbonate} = 0$ pmC, $A_{soilCO2} = 85$ pmC.

Sample	Depth	A (pmC)	δ ¹³ C	HCO₃ (m)	CO ₂ (M)	Uncorrected age (y)	Corrected age [Tamers model] (y)
L1	14.60	23.1	-10.80	0.00407	0.00005	7 470	3 569
L2	19.50	18.4	-9.60	0.00379	0.00008	8 762	4 902
L4	26.50	16.31	-10.60	0.00394	0.00008	9 460	5 598
L5	28.50	12.78	-5.50	0.00374	0.00007	10 857	6 996
L6	33.00	17.44	-2.10	0.00395	0.00006	9 076	5 192
L7	37.00	15.2	-10.70	0.00387	0.00012	9 867	6 068
L8	38.50	11.7	-11.20	0.00400	0.00010	11 363	7 529
L9	49.00	7.47	-11.10	0.00380	0.00008	13 934	10 073
L10	59.00	4.5	-10.90	0.00354	0.00007	16 787	12 926

6.3 MYLOR INVESTIGATION SITE

6.3.1 MAJOR CHEMISTRY AND ISOTOPES

Figure 6.8 shows the measured TDS, Cl⁻, δ^2 H and pH profiles with depth at the Mylor investigation site.

The TDS and Cl⁻ depth profiles are quite similar, both having significantly lower concentrations in the upper two piezometers than in the deeper two. The Cl⁻ concentrations increase by ~70% between the two shallower piezometers at 14.6 and 27 m, and the two deeper ones at 45 and 62 m, while TDS increases by ~50% across this depth range.



Figure 6.8 TDS, Cl⁻, δ^2 H, pH and profiles sampled at the Mylor investigation site, November 2006. The error bars represent the piezometer screen length from which the sample was taken.

The δ^2 H results show a trend of increasing depletion with depth. The aquifer pumping tests show there to be very little hydraulic connection between depths at this site, so any parameters that display a clear trend with depth in these piezometers is considered to be coincidental rather than evidence of greater residence time or temporal changes in recharge conditions.

The pH is ~8.1 at three of the four depths, but is 11.5 at 27 m. This is probably an anomalous result caused by contamination of the groundwater by cement in this piezometer.

The relationships of major ion (Ca²⁺, Mg²⁺, Na⁺, K⁺, SO₄²⁻ and HCO₃⁻) concentrations with the Cl⁻ concentration and their proximity to the respective seawater ion/ Cl⁻ relationship are shown in Figure 6.9.

Most of the ion/Cl⁻ ratios plot above the seawater ion/Cl⁻ dilution line, indicating that the groundwater has gained solutes from water-rock interactions. The exception to this is the Mg/Cl relationship in the 27 m sample. At that depth, a degree of ion exchange appears to have occurred that has caused the water to lose Mg and gain K. This may be related to the unusually high pH found in that piezometer. Apart from this feature, all samples follow a similar pattern to the TDS differences with depth; the 45 and 62 m samples have ion concentrations ~40–80% higher than the 13 and 27 m samples.

6.3.2 CARBON-14 AND CHLOROFLUOROCARBONS

The CFC-12 concentrations for the Mylor investigation site (Fig. 6.10) show considerable variation with depth. While the shallowest sample at 13 m appears to be older than water at 27 and 45 m, there is a linear age gradient between 27–62 m. The greater age at 13 m implies that groundwater at that depth (and above) does not flow downwards to the 27 and 45 m depths. This concurs with the findings of the aquifer pumping tests, which showed no hydraulic connection between the depths of all four piezometers at this location.

The ¹⁴C activities (Fig. 6.11) range from ~20 to ~40 pmC, with a general trend of decreasing activity with depth. The corrected ages (Fontes & Garnier 1979 correction model, Table 6.3) indicate that the oldest groundwater is that at 13 m depth and that the ages range from ~3000 to ~5000 years. The conflict between these ages and the CFC-12 ages may be due to dissolution of fossil carbonates, which would artificially increase the age indicated by ¹⁴C activity.

Table 6.3 Uncorrected and corrected ¹⁴C ages for samples from the Mylor investigation site. Corrected ages are derived using the Fontes and Garnier (1979) correction model. Data on the sample δ^{13} C and HCO₃, and CO₂ molar concentrations are used in the correction model. The values of both the δ^{13} C and ¹⁴C activities of the FRA carbonates and soil CO₂ are also used in the correction model. Values used here were: $\delta^{13}C_{carbonate} = -7.8^{\circ}/_{oo}, \delta^{13}C_{soilCO2} = -13^{\circ}/_{oo}, A_{carbonate} = 0 \text{ pmC}, A_{soilCO2} = 85 \text{ pmC}.$

Sample	Depth	A (pmC)	δ ¹³ C	HCO ₃ (m)	CO ₂ (m)	Uncorrected age (y)	Corrected age [F & G model] (y)
M1	13.0	38.8	-14.30	0.00400	0.00008	4 491	5 060
M3	45.0	18.5	-9.70	0.00720	0.00011	8 734	3 033
M4	62.0	24.7	-11.00	0.00625	0.00010	7 079	3 946

The ¹⁴C analysis of the 27 m sample was unsuccessful due to insufficient carbonate in the sample. This may be related to the unusually high pH found at that depth.



Figure 6.9 Composition diagrams of major ions versus CI[°] sampled at the Mylor investigation site in November 2006. The dashed line is the dilution line for the respective ion/CI[°] ratio in seawater. Piezometer mid-screen depths are shown beside each point.



Figure 6.10 Depth profile of CFC-12 concentrations and CFC-12 apparent ages of groundwater from the piezometers at the Mylor investigation site in November 2006. At the time samples were taken, standing water levels were 3.5 m below surface in M1 and M2, 1.91 m in M3 and 0.51 m in M4. The error bars represent the piezometer screen length from which the sample was taken.



Figure 6.11 Depth profiles of ¹⁴C activities and ¹⁴C apparent ages from the piezometers at the Mylor investigation site, November 2006. The error bars represent the piezometer screen length from which the sample was taken.

7. VERTICAL FLOW RATES AND AQUIFER RECHARGE

7.1 STABLE ISOTOPES OF WATER

The isotopic signatures of the groundwater samples from the Forreston, Fox Creek and Mylor investigation sites all plot to the left of the mean weighted rainfall for Adelaide ($\delta^2 H = -$ 4.4‰ and δ^{18} O = -23.8‰; Fig. 7.1) and above the local meteoric water line (based on local Adelaide rainfall events). This implies that recharge of the groundwater at these sites occurs during the winter months as the isotopic signatures of winter rainfall are typically depleted with respect to the mean. At all three locations there is some enrichment of $\delta^2 H$ in the shallower piezometers compared to the deeper ones. This is more apparent in the plot of $\delta^2 H$ against chloride (Fig. 7.2). Cl⁻ concentrations are approximately the same at all depths, but the $\delta^2 H$ ratio varies, with more depleted values at greater depths. This pattern suggests either that groundwater at the shallower depths has been subject to more evaporation prior to recharge, or that the groundwater at greater depths has been recharged during conditions in which winter recharge is more dominant. The isotopic ratios fall into three distinct groups for the three sites, with Fox Creek samples being more isotopically depleted than Mylor samples, and Forreston samples being the most enriched of the three groups. This variation between locations probably reflects differences in the isotopic signatures of rainfall in each location, caused by differences in altitude of the rainfall, and the nature of the recharge process, which may be more summer or winter-dominant in some areas compared to others.

Plotting δ^2 H against Cl⁻ illustrates that isotopic differences between the three sites and within the three sites are probably not due to evaporation during recharge (Fig. 7.2). While samples from the Fox Creek and Mylor sites have higher Cl⁻ concentrations than samples from the Forreston site, they are isotopically depleted. Also, among the samples at each location, there is no trend of increasing Cl⁻ concentration with increasing enrichment. The only apparent trends are an enrichment of δ^2 H with depth at each location and an increase in Cl⁻ concentration with depth at the Mylor site (sample depths are shown as a figure against each data point in Figs 7.1 and 7.2).

7.2 CARBON-14 AND CHLOROFLUOROCARBONS

7.2.1 FORRESTON INVESTIGATION SITE

Due to contamination of groundwater at the Forreston site with CFCs from a nonatmospheric source, the CFC-12 data from this site cannot be used to determine the groundwater age gradient required to derive a recharge estimate from the parallel plate model. Furthermore, the high ¹⁴C activities found in these samples indicates that they are affected by atmospheric ¹⁴C from the post-thermonuclear testing period, making them unsuitable for groundwater age-dating to provide a groundwater age gradient for the ¹⁴C vertical plate recharge model. However, if the sources of both the ¹⁴C and CFC-12 found at

VERTICAL FLOW RATES AND AQUIFER RECHARGE



Figure 7.1 Isotopes δ^2 H and δ^{18} O of groundwater samples at the Forreston, Fox Creek and Mylor investigation sites. The LMWL for Adelaide is δ^2 H = 7.7, δ^{18} O = 9.9. Adelaide rainfall samples are from GNIP, Adelaide (-34.93, 138.58), 43 m AHD, taken between 1962 and 1976. The mean weighted rainfall for Adelaide is δ^2 H = -23.8‰ and δ^{18} O = -4.4‰. Piezometer mid-screen depths are shown beside each point.



Figure 7.2 δ²H versus Cl⁻ of the groundwater samples collected at the Forreston, Fox Creek and Mylor investigation sites. Rainfall samples collected at Mount Pleasant stream gauge station (Apr-2003, Oct-2003, Mar-2005) and Echunga pluviometer (Oct-2003, Feb-2005, Jun-2005). Piezometer mid-screen depths are shown beside each point.

all piezometer depths are from recent decades (post-thermonuclear testing and during CFC-12 production), we can ascribe a maximum age to the water at all depths: 41 years for the CFC-12 concentrations and ~50 years for the 14 C activities.

There is a fairly linear increase in CFC concentration with depth, suggesting that CFC is dispersing from a source close to the surface. If a maximum age of 41 years is assumed for this source, then the age gradient between the watertable and the deepest piezometer at 63.5 m below the watertable is 0.65 y/m (41 y/63.5 m). Using equation 4.6, the average equivalent fracture aperture, determined from aquifer tests carried out on the nested piezometers, is 103 μ m with a groundwater velocity through the fractures of 4.9 m/d. A mean fracture spacing of 0.013 m and an average bulk hydraulic conductivity of 6.5 m/d was applied according to outcrop measurements and the single-well aquifer pumping tests conducted at the site. Values of matrix diffusion coefficient and matrix porosity were assumed to be 10⁻⁴ m²/y and 0.02, respectively. The values are the same as those used in the investigation by Love et al. (2002) in the Clare Valley where the targeted geology type was the Saddleworth Formation. The latter is dominated by siltstone, shale and dolomite, and has similar lithological characteristics to the Woolshed Flat Shale found at the Forreston investigation site.

To apply the parallel plate model in this case, the growth rate of CFC-12 was assumed to be zero to reflect a constant CFC-12 source. Applying the parallel plate model (equations 4.3 and 4.4), and using the parameter values listed above, the average vertical flow rate in the fracture is 0.013 m/d and the aquifer recharge rate is 44 mm/y.

If the 50 years maximum age for the ¹⁴C activity in the deepest piezometer is applied in the parallel plate model, with the aquifer parameters as above, the vertical ¹⁴C groundwater age/depth gradient of 0.79 y/m results in an average vertical flow rate in the fractures of 0.010 m/d and an aquifer recharge rate of 38 mm/y.

The accuracy of the parallel plate model depends largely on the estimated fracture spacing, matrix porosity and matrix diffusion coefficient, and to a lesser extent the hydraulic conductivity (Cook & Simmons 2000). In the application of the model here, it is even more dependent on the assumed age of the groundwater at depth, for which we have assumed a maximum age of 40–50 years. As this is a maximum age for the groundwater, providing the minimum possible age gradient, the results of 44 and 38 mm from the CFC-12 and ¹⁴C methods, respectively, must be considered to be minimum recharge rates. If the groundwater age at 63.5 m below the watertable is instead assumed to be only 20 years, then the resulting recharge rate for both the CFC-12 and ¹⁴C parallel plate models becomes 94 mm/y.

The CMB method provides a further option for the determination of recharge rates at this site (section 7.2). While recharge estimates using the CMB method alone may be questionable in many cases, the CFC-12 and ¹⁴C results are useful in supporting CMB recharge estimates determined for this site. The high ¹⁴C activities indicate that there is young groundwater, of less than 50 years, to a depth of 74 m. The high CFC concentrations at that depth also indicate that if there is a source of CFC-12 close to the surface near this site, and that CFC-12 is dispersing downward from that source, then it has reached a depth of 74 m since the source was first located here. Also, the uniform distribution of the ¹⁴C activities with depth and the consistent gradient of the CFC-12 concentrations with depth suggest the flow of groundwater here is predominantly downward through unconfined fractures. For water to have reached a depth of 74 m in less than 50 years, it must be infiltrating rapidly to this depth, reducing the likelihood of chloride contamination from water–rock interactions. These

findings suggest that if chloride concentrations of samples from these wells are used to determine recharge with the CMB method (section 7.2.1), the resulting recharge probably accurately reflects direct recharge occurring in the locality of the well.

7.2.2 FOX CREEK INVESTIGATION SITE

The ¹⁴C results from the Fox Creek investigation site produce a consistent trend of increasing age with depth, from 3500 years at 14.6 m depth to ~13 000 years at 59 m depth, when ages are corrected using the Tamers correction model. The resulting age gradient is 204 y/m. In the vertical plate recharge model, average fracture apertures and fracture spacings of 65 µm and 80 mm, respectively, were used, according to measurements made at outcrops close to the Fox Creek site. Values for the matrix porosity and diffusion coefficient were the same as used for the Forreston site due to the similarity in rock types. These are the same as at the Clare Valley site where the values were measured (Love et al. 2002). The resulting recharge rate according to the model is 0.1 mm/y. This is effectively a zero recharge rate within the accuracy of the parallel plate model. This may be indicative that recharge does not occur locally at this site but that groundwater arrives at this location via an intermediate flow system. This hypothesis is supported by the hydraulic potential measurements at this site, which show that there is an upward gradient in the groundwater head. Furthermore, the groundwater at this location is artesian during the wetter part of the year, which would prevent recharge from occurring locally.

In view of the estimated age of the water here, the absence of significant CFC-12 concentrations in the majority of samples is to be expected. Only the shallowest piezometer (14.6 m) shows a measurable CFC-12 concentration that could be used to derive an age gradient between the watertable and that depth for use in the vertical plate recharge model. Furthermore, the presence of a small amount of CFC-12 conflicts with the ¹⁴C date for this depth by ~3500 years. Either the CFC-12 result for the 14.6 m piezometer was affected by atmospheric CFC contamination during sampling, or the ages indicated by the ¹⁴C method are incorrect, perhaps because the Tamers correction model has not sufficiently corrected for dissolution of fossil carbonates. If the latter is true, a groundwater age gradient can be derived from the 38-year CFC-12 age at 14.6 m depth over the 14 m from there to the watertable and applying the resulting gradient (2.7 y/m) to the CFC-12 vertical plate recharge model. The resulting recharge rate is 4.0 mm/y. However, as the application of the parallel plate model here is reliant on the age gradient between the 14.6 m piezometer and the watertable depth, this result is only valid if groundwater occurring here is recharging locally, which does not appear to be the case.

If the groundwater found at this location recharges elsewhere and arrives here via an intermediate or regional flow system, the CMB method may be the best way to estimate the recharge rate of water found at this location (section 7.2.2).

7.2.3 MYLOR INVESTIGATION SITE

The ¹⁴C results for this investigation site show no clear age gradient with depth. The corrected ¹⁴C ages (according to the Fontes & Garnier model, Table 6.3) show the water decreasing in age between 13–45 m depth, and then increasing between 45–62 m, while the uncorrected ages show the converse of this. Aquifer pump testing at the Mylor investigation site show that there is no hydraulic connection between the four depths of the piezometers.

Measurements of piezometric head levels also show that there is an upward hydraulic gradient between these depths. It can therefore be surmised that there is no downward flow of localised recharge between these depths and that groundwater arrives at this location via an intermediate or regional flow system. The parallel plate model is therefore not applicable between the depths of the piezometers at this site. However, we can apply the model using the age gradient between the watertable and the shallowest piezometer at 13 m depth if we assume that the aquifer is unconfined at that depth.

According to measurements made at outcrops close to the Mylor site, average fracture apertures and fracture spacings of 16 μ m and 50 mm, respectively, were used in the vertical plate recharge model. Values used for the diffusion coefficient and matrix porosity were 10^{-3} m²/y and 0.05, respectively. These are significantly higher than the values of these parameters at the other two investigation sites, intending to reflect the greater porosity of the Aldgate Sandstone matrix at this location. The corrected ¹⁴C age (Fontes & Garnier correction) in the 13 m piezometer is 5060 years, and the ¹⁴C age gradient between the watertable at 2.7 m and the 13 m piezometer is 491 y/m (5060 years over 10.3 m). The resulting recharge rate according to the model is 0.38 mm/y. Within the accuracy of the parallel plate model, this is effectively a zero recharge rate. This result confirms that recharge of the groundwater at this site, even at 13 m depth, does not occur locally but arrives at this location via an intermediate flow system.

The CFC-12 age derived for the 13 m piezometer is 41 years, based on a very low CFC-12 concentration of 26 pg/kg. The resulting CFC-12 age gradient between the watertable and this piezometer is 4 y/m (41 years over 10.3 m). Using the same values for the aquifer parameters as in the ¹⁴C calculation above, the parallel plate model produces a recharge rate of 12 mm/y. However, this is based on a very low CFC-12 concentration in the sample from this piezometer. Considering the large discrepancy between the CFC-12 age of 41 years and the corrected ¹⁴C age of 5060 years, it may be that the small amount of CFC in this sample was a result of contamination with atmospheric CFC during sampling.

If the groundwater found at this location recharges elsewhere and arrives here via an intermediate regional flow system, the CMB method may be the best way to estimate the groundwater recharge rate at this investigation site (section 7.2.3).

7.3 CHLORIDE MASS BALANCE

Estimates of recharge using the CMB method have been made using Cl⁻ concentrations of samples from each piezometer at the investigation sites (Fig. 7.3). The rainfall Cl⁻ concentration is derived from an average of Cl⁻ in rain collected in pluviometers at Mt Pleasant and Echunga between 2002–05. The Mount Pleasant Cl⁻ average is used for the Forreston and Fox Creek CMB calculations and the Echunga average is used for Mylor CMB calculations. A runoff fraction of 10% of rainfall was assumed in these calculations.

7.3.1 FORRESTON INVESTIGATION SITE

The groundwater age indicators at the Forreston investigation site (section 7.1.1) show that water is young at all of the depths sampled, and probably less than 50 years old. All major ions in these samples show a similar relationship to Cl⁻, indicating a common flow path for water at all depths and suggesting vertical flow at this location. These are ideal conditions for



Figure 7.3 Vertical distribution of recharge estimates according to the CMB method at the Forreston (a), Fox Creek (b) and Mylor (c) investigation sites

the application of the CMB method, and provide some confidence in estimates of contemporary recharge rates using the method at this site. The recharge estimates, according to the CMB method, at the Forreston investigation site decreased with depth ranging from 61 mm at 16.5 m depth to 47 mm at 74 m depth. The latter corresponds closely to the CFC-12 parallel plate model recharge estimate that assumes groundwater in the 74 m piezometer is 41 years old. The apparent trend of increase in recharge rate at shallower depths suggests either that recharge has steadily increased in the past 40–50 years, or that there is some change of the groundwater CI⁻ concentration at greater depth due to longer residence time. In either case, the estimate of 61 mm at the depth of the 16.5 m piezometer is considered to be the closest to the present-day recharge rate.

The SA Geodata drillhole database contains details of 157 wells with known groundwater Cl⁻ concentrations in the ORC and TRC (Fig. 7.4). Of these, 18 are in the same geological formation as the Forreston investigation site. When the CMB recharge method is applied to the data for these wells, using an average Cl⁻ concentration from the Mount Pleasant and Echunga pluviometers of 7.9 mg/L, the 18 resulting recharge estimates have a mean of 66 mm/y and a median of 50 mm/y. The proximity of this average to the Forreston CMB recharge estimate of 61 mm/y reinforces the credibility of that estimate.

7.3.2 FOX CREEK INVESTIGATION SITE

For the Fox Creek investigation site, the CMB method was applied using the same values for the runoff fraction and the rainfall concentration as for the Forreston site. The resulting recharge estimates, illustrated in Figure 7.1, are considerably lower than those at the Forreston site, ranging from 21 mm/y at 14.6 m depth, to 17.3 mm/y at 59 m depth. However, the groundwater age indicators show groundwater at this site to be relatively old and increasing in age significantly with depth, suggesting that if there is a vertical displacement of recharging water, then recharge rates are low. However, the age of the groundwater here also means that the CMB method of recharge estimation provides an estimate of recharge



during conditions that were present thousands of years ago, at which time surface vegetation and climate may have been considerably different from current conditions. If these CMB recharge estimates are to be used, then the figure of 21 mm/y resulting from the youngest water nearest the surface would be the more representative of present-day recharge.

SA Geodata has data for only three wells with known groundwater Cl⁻ concentrations in Saddleworth Formation in the ORC and TRC (Fig. 7.4). The CMB recharge estimates based on the chloride concentrations in these three wells have a mean of 13.9 mm/y and a median of 14.6 mm/y.

A recharge estimate of 15 mm/y was determined using CFC-12 and ¹⁴C in a parallel plate model for a DWLBC investigation site in the Burra Creek Catchment (Banks et al. 2007), also in Saddleworth Formation geology. However, rainfall is considerably lower in that catchment compared to the Fox Creek site. If the Burra Creek recharge estimate is scaled up according to the difference in rainfall between that catchment and the Fox Creek site, the result is a comparative recharge estimate of 25.5 mm/y.

7.3.3 MYLOR INVESTIGATION SITE

At the Mylor site, the CMB recharge estimates range between 13 mm/y at 62 m depth and 20 mm/y at 27 m depth. The poor hydraulic connection between different depths at the site suggests that lateral flow of groundwater is present and that recharge may occur in another area. Sampling from this location shows significantly differing major chemistry in water at each depth, indicating that significant water–rock interaction processes may have occurred which may have affected Cl⁻ concentrations. As a result, the CMB method may be inaccurate in estimating recharge rates.

The investigation well at Mylor is in Aldgate Sandstone (Burra Group). SA Geodata has data for 14 wells with known groundwater Cl⁻ concentrations in Burra Group sandstone in the ORC and TRC (Fig. 7.4). The CMB recharge estimates based on the recorded Cl⁻ concentration for these wells have a mean of 114 mm/y and a median of 119 mm/y. This average may provide a more accurate indication of the recharge rate in this geology type within the WMLR catchments than CMB estimates based on Cl⁻ concentrations at the Mylor investigation site. While it is not recommended that this average be taken as the recharge rate for the Mylor site, it may be reasonable to use this as a value on which to base recharge estimates for other areas of similar geology in the WMLR. The groundwater wells that provide this average are all located between Bridgewater and Summertown, where annual rainfall is ~1000 mm/y. Most other areas in the WMLR have lower annual rainfall. A scaling of the average of 114 mm/y according to rainfall may provide a reasonable approximation of recharge in areas of the WMLR within Burra Group geology. For the Mylor investigation site where rainfall is 850 mm/y, the scaled recharge approximation is 114 mm/y x 850/1000 = 97 mm/y.

8. HORIZONTAL FLOW VELOCITIES

This chapter describes the horizontal flow velocities according to measured Radon-222 (²²²Rn) concentrations at the Forreston, Fox Creek and Mylor investigation sites. An understanding of horizontal flow rates is important to the estimation of groundwater recharge rates because the derivation of recharge rate from the age of groundwater at a depth is affected by the pathway that the groundwater has taken to reach that depth.

8.1 FORRESTON INVESTIGATION SITE

²²²Rn concentrations prior to purging range from 2.1 to 104 Bq/L (Fig. 8.1), with the high values at two distinct depths of 22–25 and 74 m. The relatively high ²²²Rn concentrations indicate that there is some active groundwater movement through the screens at those depths. At all other depths, the unpurged ²²²Rn concentrations are very low. ²²²Rn concentrations increased significantly after purging, ranging from 82 to 209 Bq/L. The purged samples represent groundwater sourced directly from the aquifer. The high purged ²²²Rn values at some depths, which were very low prior to purging, indicate that horizontal flow at those depths is very low. Conversely, the relatively small difference in the purged ²²²Rn concentrations at depths that had high ²²²Rn concentrations prior to purging indicates relatively high horizontal flow rates. This is apparent in the graph of unpurged to purged (C/Co) ²²²Rn ratios (Fig. 8.1). The variation in purged ²²²Rn concentrations with depth most likely reflects differing mineralogy and the physical characteristics of the fracture(s) intersecting the piezometer screens.

Using equation 4.9, the horizontal flow velocities at each of the sampled piezometers were calculated. The three depths with relatively high C/Co ratios are shown to have flow velocities of 8, 11 and 67 m/y. These findings suggest that there is a significant fracture intersecting the piezometer screen at ~22 m depth, and less significant fractures intersecting the screens at depths of 26 and 74 m. At all other depths, the horizontal flow rates are close to zero, which supports the suggestion that the majority of groundwater flow at this location is vertical in response to direct local recharge.

8.2 FOX CREEK INVESTIGATION SITE

²²²Rn concentrations prior to purging range from 1.8–15.6 Bq/L, with an increase in concentrations observed between 30–40 m depth (Fig. 8.2). Concentrations after purging range from 23–65 Bq/L, with the highest concentrations occurring in the uppermost piezometers between 15–20 m depth. The resulting ratios of ²²²Rn concentrations before and after purging (C/Co) show a fairly steady increase with increasing depth from 15–40 m, but then abruptly decrease at depths below 40 m. The corresponding horizontal flow rates, calculated using equation 4.9, display a similar pattern of increase towards 40 m depth to a maximum horizontal flow rate of 18.8 m/y at 38.5 m depth. Below this there is an abrupt decrease in horizontal flow, which may be indicative of a discontinuity between fractures above and below 40 m depth.



Figure 8.1 Horizontal flow rates at the Forreston investigation site derived from ratios of unpurged (C) to purged (Co) ²²²Rn concentrations in piezometers. Error bars show length of screen interval.



Figure 8.2 Horizontal flow rates at the Fox Creek investigation site derived from ratios of unpurged (C) to purged (Co) ²²²Rn concentrations in piezometers sampled during March 2006 (purged samples) and October 2006 (unpurged samples). Error bars show length of screen interval.

Aquifer testing at this site shows there is strong hydraulic connection between all the piezometer depths. The results of the ¹⁴C and CFC-12 recharge models indicate it is unlikely that any direct recharge occurs at this location, implying that the groundwater here arrives via an intermediate regional flow system. The ²²²Rn analyses indicate that this flow is primarily between 30–40 m depth. The strong hydraulic connection from 14–60 m allows inflowing water to be transmitted throughout this depth range.

8.3 MYLOR INVESTIGATION SITE

Concentrations of ²²²Rn prior to purging range from 1–5.9 Bq/L, with the highest value occurring in the shallowest piezometer at 13 m depth (Fig. 8.3). Aquifer testing shows that there is no connection between groundwater at the depths of the four piezometers in this well. The ratios of ²²²Rn concentrations before and after pumping (C/Co) show minimal variation between these four depths. The resulting calculated horizontal flow rates are low at all four depths, with a maximum flow rate of 2.5 m/y at 13 m. These low flow rates concur with the results of the aquifer testing, which showed very low transmissivity values at all piezometer depths.



Figure 8.3 Horizontal flow rates at the Mylor investigation site derived from ratios of unpurged (C) to purged (Co) ²²²Rn concentrations in piezometers sampled during November 2006. Error bars show length of screen interval.
9. CONCLUSIONS AND RECOMMENDATIONS

Hydrochemistry, isotopes, CFCs and radiogenic tracer profiles, together with geological mapping and aquifer tests, carried out at the Forreston, Fox Creek and Mylor investigation sites in the ORC and RTC, have been used to characterise groundwater flow processes and determine estimates of aquifer recharge.

The aquifer tests at the **Forreston** site indicate a freely flowing FRA at the depths of all piezometers. The EM flowmeter results also indicate there are conducting fractures at all depths under pumped conditions. The results of horizontal flow models based on ²²²Rn activities show that the wells intercept fractures at ~22–25 m depth that, under normal conditions, conduct a significant horizontal flow of ~67 m/y. A lesser flow of 8–11 m/y occurs at 74 m depth, but there appears to be negligible horizontal flow at other depths.

The CFC-12 parallel plate model indicates that if the water at 74 m depth has an age of 40 years, the recharge rate at the Forreston site is 44 mm/y. This can be considered the minimum of the range of possible recharge rates for this site. The CMB recharge estimate is slightly greater at 47 mm/y for the 74 m depth, with higher values at shallower depths. The agreement of the CMB and CFC-12 models suggests that the CMB method is providing a good indication of recharge rates. The more recently recharge water closer to the surface has Cl⁻ concentrations that result in higher CMB recharge estimates. In view of the very similar hydrochemical compositions throughout the depths sampled here, it is reasonable to assume the change in Cl⁻ concentrations with depth is due to changes in the recharge rate over time. The CMB estimate of 61 mm/y for the most recent (shallowest) recharge is the best approximation of the contemporary recharge rate at this site.

At the **Fox Creek** investigation site, the aquifer tests show very strong hydraulic connection between all depths, although the aquifer here is artesian during the winter, implying that it is confined above the shallowest piezometer (14.6 m). In view of this finding, together with the observed upward hydraulic gradient between the deepest and shallowest piezometers, it is surmised that there is no downward flow and therefore no local recharge to the FRA at this location. The water at Fox Creek appears to be very old, with ¹⁴C ages showing a minimum age of ~3600 years and a linear age/depth gradient of 204 y/m. Water arrives in this aquifer via an intermediate flow system, with a long travel time since being recharged. There is a horizontal flow of up to 19 m/y at a depth of ~40 m, with small horizontal flows above and below that depth. However, the apparently greater ages at greater depth imply that a slow downward flow has occurred prior to the horizontal flow of water to this location.

In view of the close agreement between the most appropriate CMB recharge estimate for this investigation site (21 mm/y), and the rainfall-scaled recharge estimate (25.5 mm/y) for the geologically similar investigation site at Burra, it is recommended that a recharge rate of 25 mm/y be adopted for the Fox Creek site.

At the **Mylor** investigation site, very low yields from the piezometers indicate poor connectivity of fractures in this aquifer. Although the piezometric head levels show a strong upward hydraulic gradient between the deepest and shallowest piezometers, the EM flowmeter data show only a small amount of flow occurring between depths under ambient conditions. Similarly, the analysis of ²²²Rn activities shows a very low horizontal flow occurring at all depths. These findings indicate that the conductivity of fractures is uniformly

low throughout this depth range, and it is likely that the majority of the small flows are horizontal, through fractures that have very few vertical connections. Because the ages indicated by CFC-12 and ¹⁴C are inconsistent at this site and the aquifer properties suggest negligible vertical connectivity, the parallel plate model was not applicable for the determination of recharge rates. However, there is a strong agreement between CMB recharge estimates for groundwater from 14 wells in a nearby area of similar geology. By scaling the mean of these recharge estimates according to the rainfall difference between the location of those wells and the location of the Mylor investigation site, a recharge estimate of 97 mm/y is derived. In view of the tendency of the CMB method to under-estimate true recharge rates, the value of 97 mm/y is recommended for resource management purposes as a suitably cautious estimate of recharge at locations with geology and rainfall similar to the Mylor investigation site.

APPENDICES

A. CHEMISTRY RESULTS

Table A.1 Major chemistry, isotopes, CFC-12 concentrations and ¹⁴C activities of the groundwater samples at the Forreston, Fox Creek and Mylor investigation sites, and rainfall samples from the Mount Pleasant and Echunga Pluviometers. Mean seawater is also shown.

							Field	d measur	ements						Labor	atory a	nalysis												
Location and sample type	Unit No.	Mid-screen depth from surface (m)	Sample ID	Collection date	DO (ppm)	Field EC (μS/cm)	рН	Redox (mV)	Temp (°C)	Field alkalinity (HCO ₃ ⁻) (mg/L)	TDS (mg/L)	Lab pH	Ca²+ (mg/L)	Mg²⁺ (mg/L)	Na⁺ (mg/L)	K⁺ (mg/L)	SO₄ ²- (mg/L)	CI ⁻ (mg/L)	Lab alkal- inity (HCO ₃ ⁻) (mg/L)	Br (mg/L) ⁻	NH₄-N (mg/L)	NO_x-N (mg/L)	Sr (ug/L)	δ ¹⁸ 0 (‰ SMOW)	<mark>δ²Η</mark> (‰ SMOW)	CFC-12 (pg/kg)	CFC-12 apparent age (y)	¹⁴ C (pmC)	δ ¹³ C (‰ PDB)
Forreston GW	6628-22357	16.5	F1	01/02/06	0.02	810	7.3	-69	18.3	144	519	7.6	25	16	115	8	79	95	180	0.24	0.037	<0.02	107	-4.94	-23.9	1710	N/A	94.3	-19.1
Forreston GW	6628-22356	22.5	F2	31/01/06	0.50	728	6.85	-47.7	18.76	156	529	7.4	23	18	117	8	73	104	185	0.28	0.025	<0.02	102	-5.03	-22.3	1252	N/A	93.3	-17.9
Forreston GW	6628-22352	25.5	F3	01/02/06	0.92	867	7.09	-52	18.7	130	558	7.6	25	18	126	8	98	102	182	0.26	0.045	<0.02	104	-4.92	-21.9	1000	N/A	97.1	-16.2
Forreston GW	6628-22355	31.5	F4	31/01/06	0.12	759	7.1	-127.1	19.03	156	560	7.5	25	18	124	9	79	110	195	0.29	<0.02	<0.02	109	-4.94	-23.6	1366	N/A	98.7	-18.2
Forreston GW	6628-22354	36.5	F5	31/01/06	0.22	780	6.64	-70.6	19	130	562	7.2	21	21	127	8	90	114	181	0.29	<0.02	<0.02	92	-4.59	-24.8	887	N/A	94.4	-17.2
Forreston GW	6628-22351	54.0	F6	01/02/06	-0.05	943	7.02	-46	18.5	162	604	7.5	28	21	133	9	89	119	206	0.28	<0.02	<0.02	108	-4.93	-24.3	439	N/A	92.2	-17.1
Forreston GW	6628-22350	61.0	F7	01/02/06	-0.08	924	7.1	-97	18.4	162	581	7.4	24	20	133	9	75	123	197	0.31	<0.02	<0.02	96	-4.99	-26.2	367	N/A	92.4	-17.0
Forreston GW	6628-22349	74.0	F8	01/02/06	-0.02	902	6.98	-42	18.4	152	571	7.4	22	20	131	8	73	122	195	0.33	<0.02	<0.02	97	-4.95	-26.1	495	N/A	90.8	-17.3
Fox Creek GW	6628-22478	14.6	L1	03/10/06	1.05	1450	8.1	132	19.17	260	855	8.2	31	28	212	10	8	302	263	0.96	0.079	0.128	1369	-5.86	-30.2	52	38	23.1	-10.8
Fox Creek GW	6628-22486	19.5	L2	03/10/06	0.61	1477	7.79	55	16.62	240	848	8.0	33	28	213	9	8	316	242	0.99	0.178	0.024	1473	-5.91	-29.9	24	>41	18.4	-9.6
Fox Creek GW	6628-22481	26.5	L4	03/10/06	0.31	1513	7.7	-21	16.65	235	867	8.0	30	26	223	9	4	324	250	1.01	0.187	0.038	1566	-5.94	-34.9	25	>41	16.3	-10.6
Fox Creek GW	6628-22484	28.5	L5	03/10/06	0.15	1521	8.04	-43	16.34	203	869	8.0	27	24	234	9	2	335	238	1.06	0.208	<0.02	1506	-5.98	-29.6	<20	>41	12.8	-5.5
Fox Creek GW	6628-22483	33.0	L6	03/10/06	0.07	1508	8.06	-182	16.29	250	870	8.1	31	27	224	9	3	323	253	1.03	0.189	<0.02	1609	-5.92	-28.8	<20	>41	17.4	-2.1
Fox Creek GW	6628-22482	37.0	L7	04/10/06	0.41	1554	7.67	-126	17.48	230	881	7.8	33	27	225	8	2	342	244	1.08	0.196	<0.02	2095	-6.1	-33.4	<20	>41	15.2	-10.7
Fox Creek GW	6628-22480	38.5	L8	04/10/06	0.53	1548	7.75	-91	16.29	238	883	7.9	28	24	235	8	2	333	253	1.03	0.217	<0.02	1522	-5.97	-34.8	<20	>41	11.7	-11.2
Fox Creek GW	6628-22479	49.0	L9	04/10/06	0.37	1557	7.8	-134	17.75	236	877	8.0	26	24	236	8	1	341	241	1.08	0.215	<0.02	1613	-6.06	-34.8	<20	>41	7.5	-11.1
Fox Creek GW	6628-22478	59.0	L10	04/10/06	0.43	1607	7.95	-125	16.92	200	887	8.0	27	24	242	9	1	359	225	1.16	0.217	<0.02	1854	-6.11	-32.7	<20	>41	4.5	-10.9
Mylor GW	6627-11286	13.0	M1	22/11/06	0.03	1554	7.75	-111	17.26	216	997	8.0	39	30	240	12	94	327	254	1.06	0.135	<0.01	224	-5.64	-26.3	26	41	38.8	-14.3
Mylor GW	6627-11285	27.0	M2	22/11/06	0.39	1905	11.7	-116	17.3	270	834	11.4	48	0	226	28	49	278	205	0.76	0.014	<0.01	482	-5.74	-27.6	179	17		
Mylor GW	6627-11284	45.0	M3	22/11/06	0.64	1954	7.28	-105	19.12	340	1430	8.1	65	49	298	10	166	369	474	1.24	0.019	<0.01	262	-5.52	-28.2	110	26	18.5	-9.7
Mylor GW	6627-11283	62.0	M4	22/11/06	0.32	2001	7.36	-91	17.32	280	1419	8.1	71	53	294	9	144	437	411	1.48	<0.01	<0.01	292	-5.68	-29	<20	>41	24.7	-11.0
Mt Pleasant pluvio				23/04/03														5.5						-5.08	-27.9				
Mt Pleasant pluvio				08/10/03														4.6						-5.69	-26.2				
Mt Pleasant pluvio				04/03/05														8.8						-3.72	-17.1				
Mt Pleasant pluvio				27/05/05														14.8						-1.78					
Echunga pluvio				08/10/03														5.7						-5.12	-21.9				
Echunga pluvio				25/02/05														10.6						-2.95	-11.1				
Echunga pluvio				24/06/05														5.2						-5.55	-25.2				
Mean seawater											35139	8.2	412	1294	10760	399	2712	19350	145	67				0	0				

Sample ID	Mid-screen depth from surface (m)	<mark>1∕₂ screen</mark> length (m)	Radon — unpurged date	Radon conc. (C) unpurged (Bq/L)	Radon error (C) (Bq/L)	Radon — purged date	Radon conc. (Co) purged (Bq/L)	Radon error (Co) (Bq/L)
Forreston								
F1	16.5	1.5	12-Oct-06	7.2	0.4	10-Oct-05	44.3	1.1
F2	22.5	1.5	12-Oct-06	1.8	0.2	10-Oct-05	65.1	1.5
F3	25.5	1.5	12-Oct-06	4.9	0.3	27-Mar-06	27.8	0.9
F4	31.5	1.5	12-Oct-06	3.6	0.3	27-Mar-06	22.9	0.8
F5	36.5	1.5	12-Oct-06	9.5	0.5	28-Mar-06	30.2	0.9
F6	54.0	2	12-Oct-06	13.7	0.6	28-Mar-06	34	1
F7	61.0	3	12-Oct-06	15.6	0.6	28-Mar-06	26.3	0.9
F8	74.0	2	12-Oct-06	1.9	0.2	28-Mar-06	20.6	0.8
Fox Creek								
L1	14.6	1.5	12-Oct-06	5.4	0.4	12-Oct-05	40.6	1.2
L2	19.5	1	01-Feb-06	6.6	0.3	01-Feb-06	209	4
L4	26.5	1.25	31-Jan-06	104	2	31-Jan-06	124	3
L5	28.5	1.5	31-Jan-06	64.3	1.7	01-Feb-06	139	3
L6	33.0	1.5	31-Jan-06	4.8	0.3	31-Jan-06	104	2
L7	37.0	1	31-Jan-06	3.6	0.3	31-Jan-06	81.9	1.8
L8	38.5	1	01-Feb-06	13.1	0.5	01-Feb-06	103	2
L9	49.0	1.5	01-Feb-06	2.1	0.2	01-Feb-06	140	3
L10	59.0	2	01-Feb-06	48	1.1	01-Feb-06	124	3
Mylor								
M1	13.0	3	22-Nov-06	5.9	0.3	22-Nov-06	36	1.2
M2	27.0	1.5	22-Nov-06	1.2	0.2	22-Nov-06	12.4	0.5
M3	45.0	1.5	22-Nov-06	1	0.2	22-Nov-06	7.9	0.4
M4	62.0	1.5	22-Nov-06	2	0.2	22-Nov-06	17	0.6

Table A.2Measured 222Rn concentrations from the unpurged and purged piezometers at the
Forreston, Fox Creek and Mylor investigation sites

B. LITHOLOGICAL LOGS

Unit No.	Permit No	Drill date	Depth from (m)	Depth to (m)	Major lithology	Minor lithology	Description
6628-22353	PN106396	08/12/2005	0	2	SLAT		Quartz–muscovite schist and quartzite with minor muscovite. Hard, silicified. Iron staining along fractures. Minor clay, hard, low plasticity, minimal topsoil.
			2	6	SLAT		Quartz-muscovite schist. Very hard, silicified. Alteration along fracture surfaces.
			6	8	SCHT		Quartz-muscovite schist. Minor weathering. Iron staining. Grey.
			8	12	SCHT		Quartz–muscovite schist. Very fine grained. Hard, brittle. Iron staining. Minor clear quartz fragments between 10–12 m. Grey.
			12	16	SCHT		Quartz–muscovite schist. Very fine grained. Iron staining. Minor opaque quartz fragments. Grey.
			16	22	SCHT		Quartz–muscovite schist. Very fine grained. Iron staining. Increased quartz vein fragments. Dark grey.
			22	28	SCHT		Quartz-muscovite schist. Very fine grained. Hard. Minor quartz vein fragments.
			28	30	SCHT		Quartz-muscovite schist. Fine grained. Minor opaque quartz vein fragments.
			30	32	SCHT		Quartz-muscovite schist. Fine grained. Minor amber quartz fragments.
			32	42	SCHT		Quartz-muscovite schist. Very fine grained. Hard. Minor opaque quartz vein fragments.

Table A.3 Forreston — River Torrens Catchment, lithological log for Forreston 203 mm well (Fr1)

Unit No.	Permit No	Drill date	Depth from (m)	Depth to (m)	Major lithology	Description
6628-22348	PN106397	09/12/2005	5 0	2	SOIL	Topsoil. Sandy clay. Weathered muscovite schist. Minor schist fragments. Minor quartz vein fragments. Light red-brown.
			2	4	SCHT	Quartz-muscovite schist. Weathered. Soft. Minor quartz. Light red-brown.
			4	8	SCHT	Quartz-muscovite schist. Weathered. Moderate-hard. Minor clear quartz fragments. Brown-grey.
			8	14	SCHT	Quartz-muscovite schist. Very hard. Minor quartz vein fragments. Dark blue-grey.
			14	16	SCHT	Quartz-muscovite schist. Very hard. Dark blue-grey. Water cut at 16 m.
			16	20	SCHT	Quartz–muscovite schist. Very hard. Quartz veins present in schist cuttings. Minor quartz vein fragments. Dark blue-grey.
			20	22	SCHT	Quartz-muscovite schist. Very hard. Minor quartz vein fragments. Dark blue-grey.
			22	26	SCHT	Quartz-muscovite schist. Very hard. Minor white-smoky grey quartz vein fragments. Dark blue-grey.
			26	28	SCHT	Quartz-muscovite schist. Very hard. Layering present in cuttings. Minor amber quartz.
			28	36	SCHT	Quartz-muscovite schist. Very hard. Abundant quartz vein fragments between 32-34 m. Dark blue-grey.
			36	46	SCHT	Quartz–muscovite schist. Pyrite on fracture and cleavage surfaces. Quartzite fragments. Possible chloritic alteration. Dark blue-grey.
			46	48	SCHT	Quartz–muscovite schist. Pyrite on fracture and cleavage surfaces. Quartz vein fragments. Minor fragments with brecciated appearance. Chloritic alteration.
			48	58	SCHT	Quartz-muscovite schist. Silicified fragments. Chloritic alteration. Quartz vein fragments.
			58	64	SCHT	Quartz–muscovite schist. Fine-grained muscovite (<1 mm). Pyrite on fracture surfaces. Minor quartz vein material. Decreased chloritic alteration.
			64	68	SCHT	Quartz-muscovite schist. Pyrite on fracture surfaces. Increased chloritically altered quartz vein material.
			68	74	SCHT	Quartz-muscovite schist. Pyrite on fracture surfaces. Decreased quartz vein material.
			74	80	SCHT	Quartz-muscovite schist. Pyrite on fracture surfaces. Increased chloritically altered quartz vein material.

 Table A.4
 Forreston — River Torrens Catchment, lithological log for Forreston 203 mm well (Fr2)

Unit No.	Permit No	Drill date	Depth from (m)	Depth to (m)	Major lithology	Minor lithology	Description
6628-22476	PN106399	24/05/2005	0	2	SOIL	CLYU	Clayey topsoil. Light red-brown. Moderate plasticity. Pliable. Moderate sheen.
			2	4	CLYU		Clay. Light red-brown. Moderate plasticity, pliable, increased moisture content, high sheen.
			4	6	CLYU	SILT	Silty clay. Light brown. Friable. Minor weathered slate fragments.
			6	8	CLYU	SILT	Silty clay. Light grey-brown. Increased weathered slate fragments.
			8	10	SLAT		Slate. Weathered. Cleavage visible in fragments. Soft. Grey.
			10	12	SLAT		Slate. Weathered. Cleavage visible in fragments. Medium-hard. Grey.
			12	14	SLAT		Slate. Weathered. Minor pyrite. Slaty cleavage. Blue-grey. High clay content in sample. Soft, pliable.
			14	16	SLAT		Slate. Weathered. Minor pyrite. Slaty cleavage. Blue-grey. Quartz vein material lining fragment surfaces. Minor iron staining. Decreased clay.
			16	18	SLAT		Slate. Well-developed slaty cleavage. Pyrite on cleavage and fracture surfaces. Grey.
			18	24	SLAT		Slate. Well-developed slaty cleavage. Possible crenulation cleavage. Pyrite on cleavage surfaces. Possible bedding; minor quartz-rich thin layers. Quartz vein material between 20–24 m. Blue-grey
			24	28	SLAT	MSST	Slate. Slaty cleavage. Possible crenulation cleavage. Thin pyrite veins. Minor quartz vein material. Blue-grey.
			28	30	SLAT	MSST	Slate. Slaty cleavage. Minor increase in metasandstone throughout cuttings. Decreased quartz vein material. Water cut at 29 m, 20 L/s — water level in adjacent 203 mm well dropped to ~8.6 m, previously flowing.
			30	39.5	SCHT	MSST	Metasiltstone interbedded with metasandstone. Metasandstone layers up to 2 mm thick. Increased pyrite on fracture surfaces.

 Table A.5
 Forreston — River Torrens Catchment, lithological log for Fox Creek 254 mm well (FC1)

Unit No.	Permit No	Drill date	Depth from (m)	Depth to (m)	Major lithology	Minor lithology	Description
6628-22475	PN106398	20/05/2005	0	2	SOIL	CLYU	Clayey topsoil. Light red-brown. Moderate density, low plasticity. Weathered slate fragments, minor quartz vein material. Manganese weathering, fragments friable.
			2	6	CLYU		Clay. Soft, pliable, low plasticity, high sheen, increased moisture content. Decreased shale fragments. Red-brown.
			6	10	SLAT	CLYU	Slate. Weathered, friable. Cleavage obvious in fragments. Grey. Clay. Red-brown. Decreased clay between 8–10 m.
			10	12	SLAT		Slate. Variable weathering. Soft, friable. Grey and light red-brown. Minor quartz vein material. Decreased weathering between 11–12 m.
			12	18	SLAT		Slate. Minor weathering. Well-developed slaty cleavage. Grey.
			18	22	SLAT		Slate. Well-developed slaty cleavage. Hard. Pyrite associated with slate and as discrete fragments. Cuttings 2–10 mm.
			22	36	SLAT		Slate. Well-developed slaty cleavage. Decreased pyrite.
			36	38	SLAT		Slate. Well-developed cleavage. Minor quartz vein fragments.
			38	40	SLAT		Slate. Well-developed cleavage. Abundant quartz vein fragments (clear, white). Slate fragments exhibit rounded surfaces.
			40	48	SLAT		Slate. Slaty cleavage. Quartz vein fragments.
			48	54	SLAT		Slate. Slaty cleavage. Quartz veins in cuttings. Pyrite and quartz vein fragments.
			54	60	SLAT		Slate. Slaty cleavage. Quartz veins. Significant pyrite in cuttings.
			60	64	SLAT		Slate. Slaty cleavage. Pyrite. Minor quartz vein material.
			64	66	SLAT		Slate. Slaty cleavage. Abundant pyrite.
			66	76	SLAT		Slate. Slaty cleavage. Pyrite. Minor quartz vein material.
			76	80	SLAT		Slate. Slaty cleavage. Minor pyrite, minor quartz vein material.
			80	90	SLAT		Slate. Slaty cleavage. Minor pyrite, minor quartz vein material.

Table A.6 Forreston — River Torrens Catchment, lithological log for Fox Creek 203 mm well (FC2)

Unit No.	Permit No	Drill date	Depth from (m)	Depth to (m)	Major lithology	Minor lithology	Description
6628-11279	PN106401	14/11/2005	0	1	CLYU		Sandy clay. Quartzite fragments. Quartz vein material. Red-orange brown.
			1	3	SAND		Sand. Weathered metasandstone. Coarse grained, poorly sorted. Friable. Minor clay fragments. Pale yellow-orange.
			3	6	CLYU	SAND	Clayey sand. Highly weathered metasandstone. Poorly sorted. Friable. Light grey.
			6	10	SAND	CLYU	Slightly clayey sand. Minor quartzite fragments. Friable. Soft. Increased clay between 9–10 m. Orange.
			10	11	MSST		Metasandstone. Very well cemented, siliceous cement. Medium grained, moderate to well sorted. Very minor opaques. Minor iron staining.
			11	19	MSST		Metasandstone. Very well cemented, siliceous cement. Medium grained, moderate to well sorted, angular. Very minor opaques. Minor schist fragments, slightly talcy appearance. Minor quartz vein material, clear angular fragments.
			19	23	MSST		Metasandstone. Moderate to well cemented, siliceous cement. Moderate to well sorted, subrounded–subangular grains. Minor opaques. Minor clear quartz vein material. Minor iron staining.
			23	25	MSST		Metasandstone. Well cemented. Well sorted. Slightly crystalline appearance. Pale green-grey.
			25	33	QTZT		Quartzite. Crystalline appearance. Very hard. Minor, fine grained opaques. Light grey-green. Minor biotite–quartz schist fragments. Silicified. Schist increasing towards 31 m. Increased quartz vein fragments between 31–33 m.
			33	37.5	QTZT		Quartzite. Crystalline. Very hard. Pale green-grey. Quartz vein fragments. Biotite– quartz schist fragments. Schist fragments decrease from 35–37.5 m.
			37.5	43.7	QTZT		Quartzite. Crystalline. Very hard. Minor muscovite–quartz schist, 0.3 m schistose layer at 43.5 m. Quartz vein fragments.
			43.7	51.7	QTZT		Quartzite. Crystalline. Very hard. Minor quartz vein material. Light green-grey. Biotite–quartz schist. Possible crenulation cleavage in schist fragments. Minor muscovite–quartz schist.
			51.7	55.8	QTZT		Quartzite. Crystalline. Very hard. Increased quartz vein fragments. Green-grey. Increased muscovite and biotite–quartz schists. Chloritic alteration of micas. Crenulation cleavage in schists.

 Table A.7
 Forreston — River Torrens Catchment, lithological log for Mylor 203 mm well

Unit No.	Permit No	Drill date	Depth from (m)	Depth to (m)	Major lithology	Minor lithology	Description
			55.8	59.8	QTZT		Quartzite. Crystalline. Very hard. Pale green-grey. Minor quartz vein material. Minor muscovite and biotite–quartz schists. Crenulation cleavage in schists. Chloritic alteration absent.
			59.8	70	QTZT		Quartzite. Crystalline. Very hard. Pale green-grey. Minor quartz vein material. Minor biotite–quartz schist. Crenulation cleavage in schist. Minor chloritic alteration. Schist fragments decrease from 61.9–70 m.
			70	72	QTZT		Quartzite. Crystalline. Hard. Pale green-grey. Minor biotite–quartz schist. Minor quartz vein material.
			72	76.1	QTZT		Quartzite. Crystalline. Hard. Pale green-grey. Abundant muscovite and biotite–quartz schists. Schists decreases towards 76.1 m. Quartz fragments.
			76.1	80.2	QTZT		Quartzite. Crystalline. Hard. Minor opaques. Pale green-grey. Quartz vein fragments. Minor muscovite and biotite–quartz schist fragments.

UNITS OF MEASUREMENT

Name of unit	Symbol	Definition in terms of other metric units	Quantity
day	d	24 h	time interval
gigalitre	GL	10 ⁶ m ³	volume
gram	g	10 ⁻³ kg	mass
hectare	ha	$10^4 m^2$	area
hour	h	60 min	time interval
kilogram	kg	base unit	mass
kilolitre	kL	1 m ³	volume
kilometre	km	10 ³ m	length
litre	L	10 ⁻³ m ³	volume
megalitre	ML	10 ³ m ³	volume
metre	m	base unit	length
microgram	μg	10 ⁻⁶ g	mass
microlitre	μL	10 ⁻⁹ m ³	volume
milligram	mg	10 ⁻³ g	mass
millilitre	mL	10 ⁻⁶ m ³	volume
millimetre	mm	10 ⁻³ m	length
minute	min	60 s	time interval
second	S	base unit	time interval
tonne	t	1000 kg	mass
year	У	365 or 366 days	time interval
~ approximately e	qual to		

Units of measurement commonly used (SI and non-SI Australian legal)

y = -	,
~	approximately equal to
δ²Η	hydrogen isotope composition
δ ¹⁸ Ο	oxygen isotope composition
¹⁴ C	carbon-14 isotope (percent modern carbon)
δ ¹³ C	dissolved inorganic carbon (DIC)
CFC	chlorofluorocarbon (parts per trillion volume)
EC	electrical conductivity (µS/cm)
SEC	specific electrical conductivity (µS/cm)
рН	acidity
ppm	parts per million
ppb	parts per billion
TDS	total dissolved solids (mg/L)

GLOSSARY

Ambient — The background level of an environmental parameter (e.g. a background water quality such as salinity).

Aquifer — An underground layer of rock or sediment that holds water and allows water to percolate through.

Aquifer, confined — Aquifer in which the upper surface is impervious and the water is held at greater than atmospheric pressure. Water in a penetrating well will rise above the surface of the aquifer.

Aquifer test — A hydrological test performed on a well, aimed to increase the understanding of the aquifer properties, including any interference between wells, and to more accurately estimate the sustainable use of the water resource available for development from the well.

Aquifer, unconfined — Aquifer in which the upper surface has free connection to the ground surface and the water surface is at atmospheric pressure.

Baseflow — The water in a stream that results from groundwater discharge to the stream. (This discharge often maintains flows during seasonal dry periods and has important ecological functions.)

Bore — See well.

Catchment — That area of land determined by topographic features within which rainfall will contribute to runoff at a particular point.

DWLBC — Department of Water, Land and Biodiversity Conservation (Government of South Australia).

EC — Electrical conductivity. 1 EC unit = 1 micro-Siemen per centimetre (μ S/cm) measured at 25°C. Commonly used to indicate the salinity of water.

EMLR — Eastern Mount Lofty Ranges.

Evapotranspiration — The total loss of water as a result of transpiration from plants and evaporation from land, and surface water bodies.

Geological features — Include geological monuments, landscape amenity and the substrate of land systems and ecosystems.

Groundwater — See underground water.

Hydrogeology — The study of groundwater, which includes its occurrence, recharge and discharge processes, and the properties of aquifers. (*See hydrology.*)

Hydrology — The study of the characteristics, occurrence, movement and utilisation of water on and below the Earth's surface and within its atmosphere. (*See hydrogeology.*)

MLR — Mount Lofty Ranges.

Model — A conceptual or mathematical means of understanding elements of the real world which allows for predictions of outcomes given certain conditions. Examples include estimating storm runoff, assessing the impacts of dams or predicting ecological response to environmental change.

Mount Lofty Ranges Watershed — The area prescribed by Schedule 1 of the regulations.

Natural recharge — The infiltration of water into an aquifer from the surface (rainfall, streamflow, irrigation etc.). (See recharge area, artificial recharge.)

Natural resources — Soil; water resources; geological features and landscapes; native vegetation, native animals and other native organisms; ecosystems.

Permeability — A measure of the ease with which water flows through an aquifer or aquitard. The unit is m^2/d .

Potentiometric head — The potentiometric head or surface is the level to which water rises in a well due to water pressure in the aquifer; the unit is metres (m).

Prescribed water resource — A water resource declared by the Governor to be prescribed under the Act, and includes underground water to which access is obtained by prescribed wells. Prescription of a water resource requires that future management of the resource be regulated via a licensing system.

Recharge area — The area of land from which water from the surface (rainfall, streamflow, irrigation, etc.) infiltrates into an aquifer. (See artificial recharge, natural recharge.)

Surface water — (a) water flowing over land (except in a watercourse), (i) after having fallen as rain or hail or having precipitated in any another manner, (ii) or after rising to the surface naturally from underground; (b) water of the kind referred to in paragraph (a) that has been collected in a dam or reservoir.

Underground water (groundwater) — Water occurring naturally below ground level or water pumped, diverted or released into a well for storage underground.

Water allocation — (a) in respect of a water licence means the quantity of water that the licensee is entitled to take and use pursuant to the licence; (b) in respect of water taken pursuant to an authorisation under s. 11 means the maximum quantity of water that can be taken and used pursuant to the authorisation.

Water allocation plan (WAP) — A plan prepared by a CWMB or water resources planning committee and adopted by the Minister in accordance with Division 3 of Part 7 of the Act.

Watercourse — A river, creek or other natural watercourse (whether modified or not) and includes: a dam or reservoir that collects water flowing in a watercourse; a lake through which water flows; a channel (but not a channel declared by regulation to be excluded from the this definition) into which the water of a watercourse has been diverted; and part of a watercourse.

Well — (a) an opening in the ground excavated for the purpose of obtaining access to underground water; (b) an opening in the ground excavated for some other purpose but that gives access to underground water; (c) a natural opening in the ground that gives access to underground water.

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